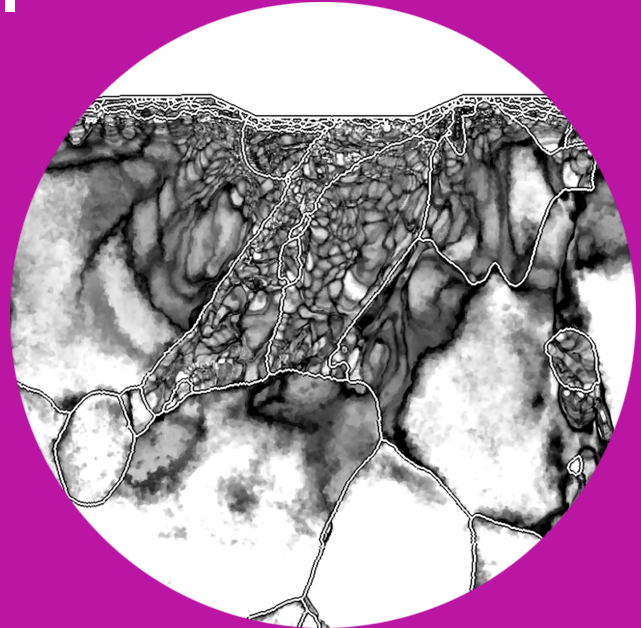


Characterisation of local plastic deformation

—
MTEX 2020 workshop



Aalto University
School of Engineering
Marine Technology



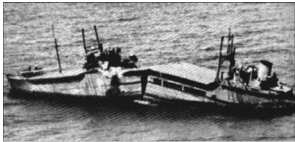
D.Sc. Pauli Lehto

10.3.2020

Contents

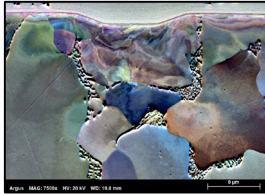
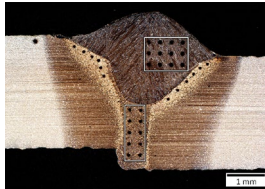
1

Introduction



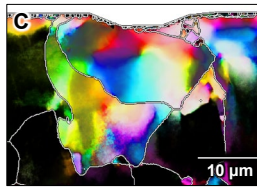
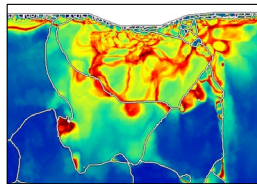
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Scope of work



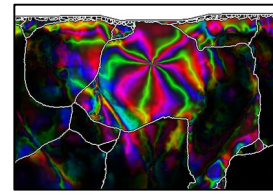
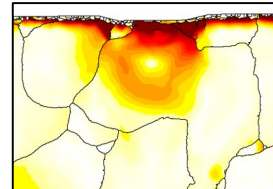
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Misorientation analysis in MTEX



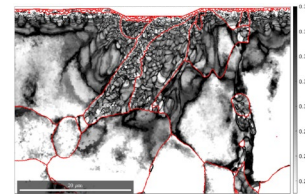
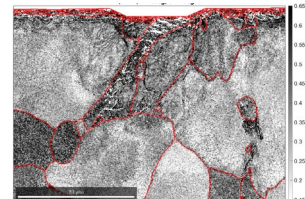
4

Analysis examples



5

Conclusions

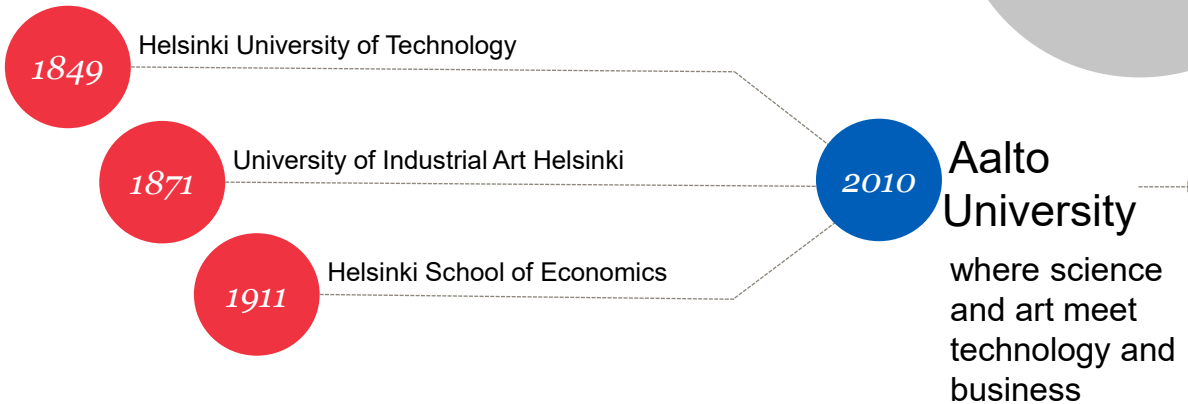


Introduction

Aalto University

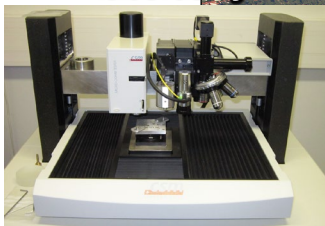
Unique merger of three leading Finnish universities
to cover cross-discipline teaching and research

*The Aalto University community:
80 000 alumni,
20 000 students,
5 000 staff members,
370 professors*



Aalto University – Otaniemi Campus

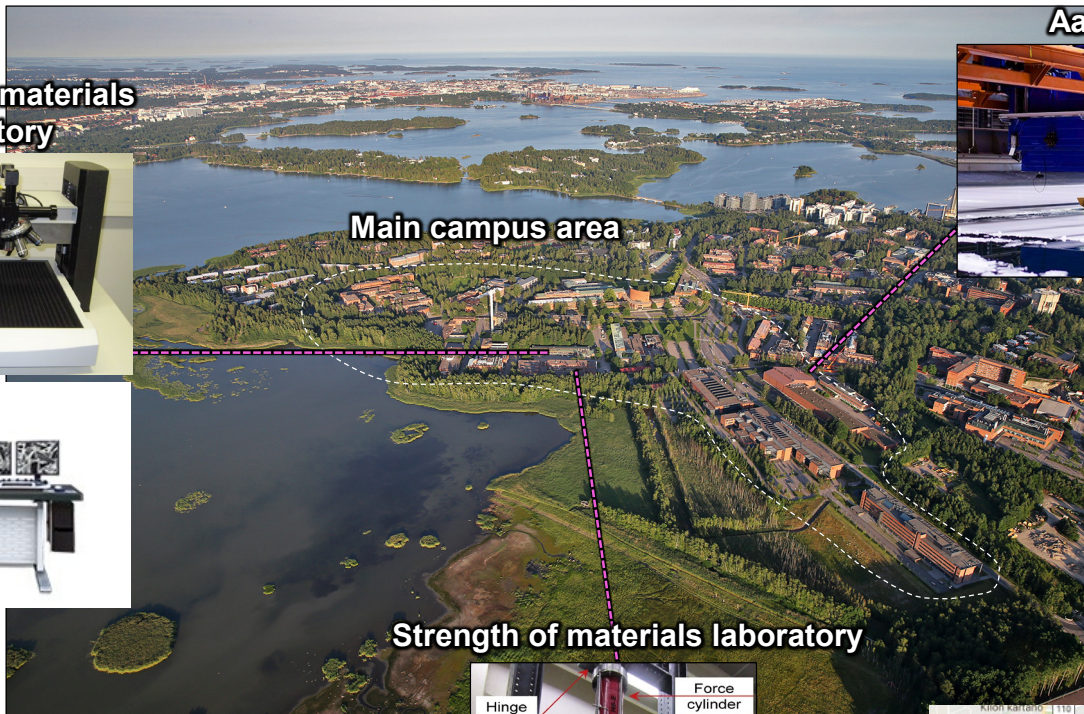
Engineering materials laboratory



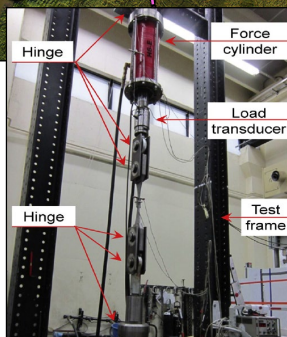
Aalto Ice Tank



Main campus area



Strength of materials laboratory



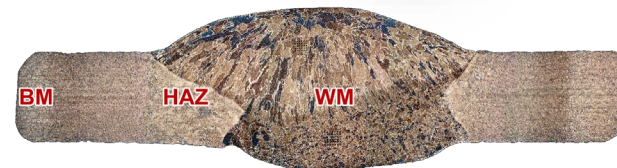
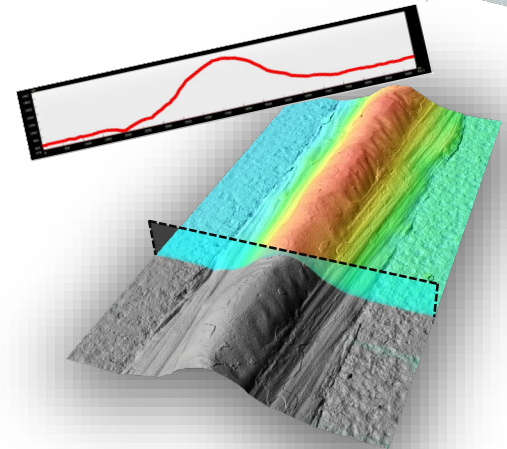
Background

Sustainable growth requires the effective use of high strength steels

- Steel's mechanical properties are affected by the manufacturing process
- Statistical analysis is required across several length scales for engineering purposes

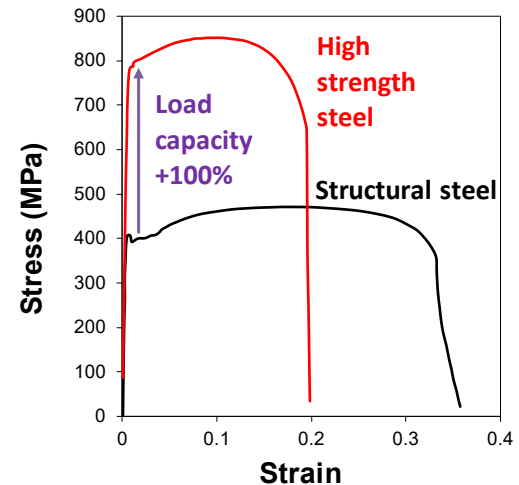
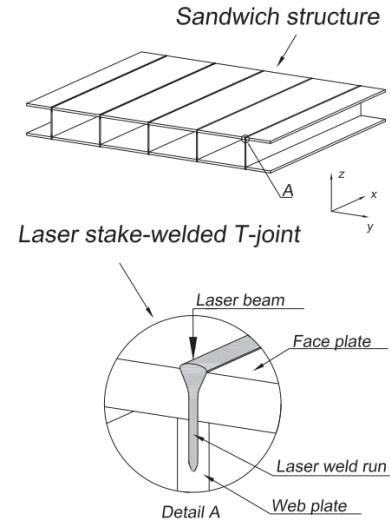
Research in the microstructural length scale reveals deformation mechanisms

- Optimisation of materials and manufacturing processes made possible by understanding the fundamental microstructure – strength relationships



Steel in shipbuilding

- Energy efficiency of ships calls for alternative structural topologies and stronger steel grades (relative density)
- New manufacturing methods need to be implemented to fully utilize the higher strength and to guarantee the safety of the structure (e.g. fatigue)
- Welds are often structural weak points prone to failure (microstructural effects)



Steel in shipbuilding

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Elastic limit
850 MPa

Allowed stress
268 MPa



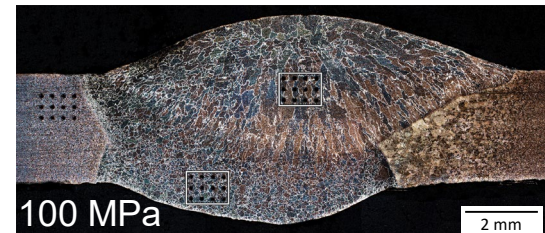
501 MPa



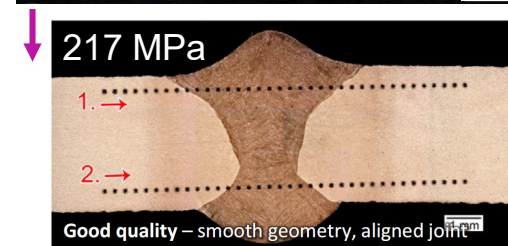
562 MPa



Elastic limit ~355 MPa



100 MPa



217 MPa

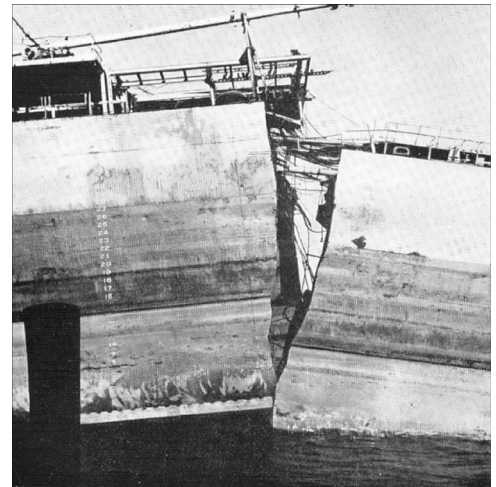
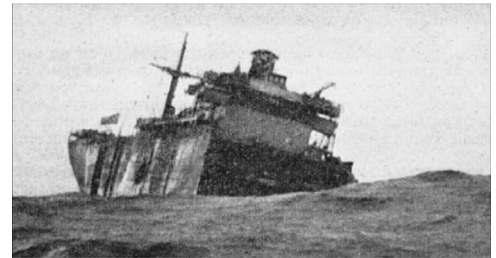
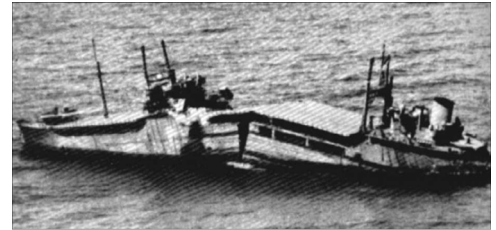
1. →

2. →

Good quality – smooth geometry, aligned joint

Steel in shipbuilding

- Energy efficiency of ships calls for alternative structural topologies and stronger steel grades (relative density)
- New manufacturing methods need to be implemented to fully utilize the higher strength and guarantee the safety of the structure (e.g. fatigue)
- **Welds are often structural weak points prone to failure (microstructural effects)**



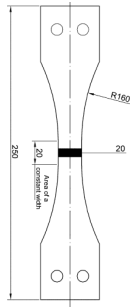
Length scales of research

- To prevent catastrophic failures, we need to understand the load carrying mechanisms in different length scales
- Fundamental question: how does the manufacturing process affect the strength properties of steel?
- How to approach the problem, top-down or bottom-up?



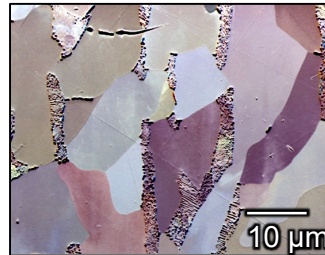
300m +

Ship
structure



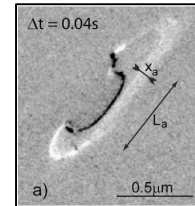
1 m ... 1 cm

Weld
detail



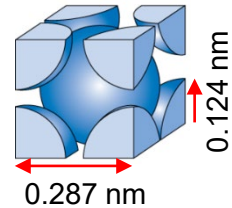
1000...1 μm

Microstructure



1 μm...100 nm

Dislocations



1 Å = 0.1 nm

Atoms

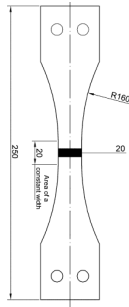
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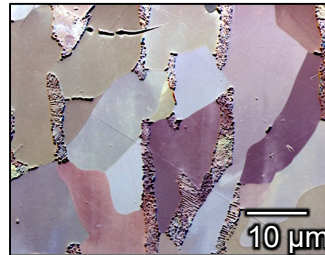
300m +

Ship structure



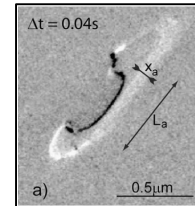
1 m ... 1 cm

Weld detail



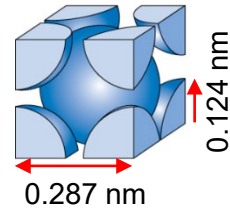
1000...1 μm

Microstructure



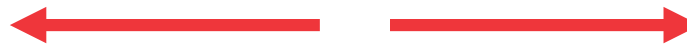
1 μm...100 nm

Dislocations



1 Å = 0.1 nm

Atoms



Length scales of research

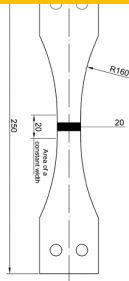
- To prevent catastrophic failures, we need to understand the load carrying mechanisms in different length scales
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Statistical variation



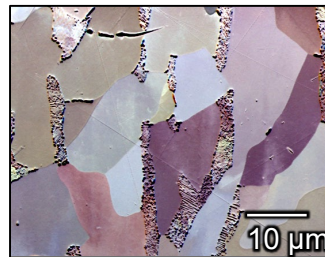
300m +

Ship
structure



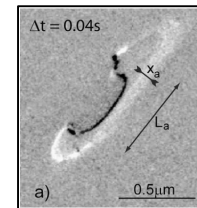
1 m ... 1 cm

Weld
detail



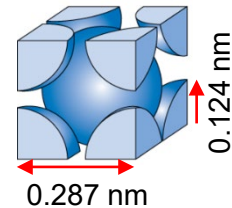
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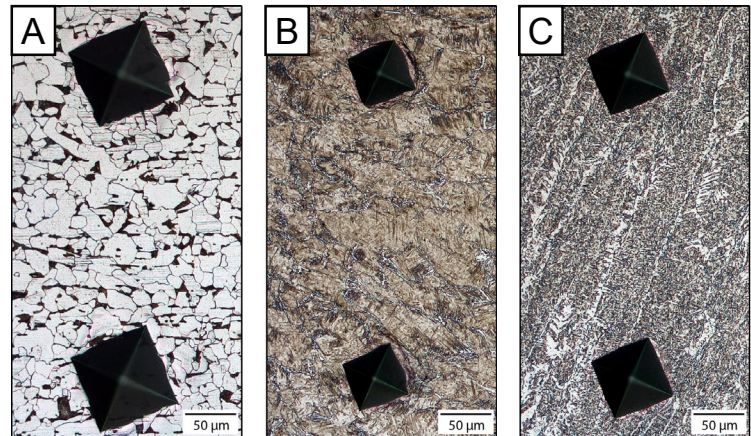
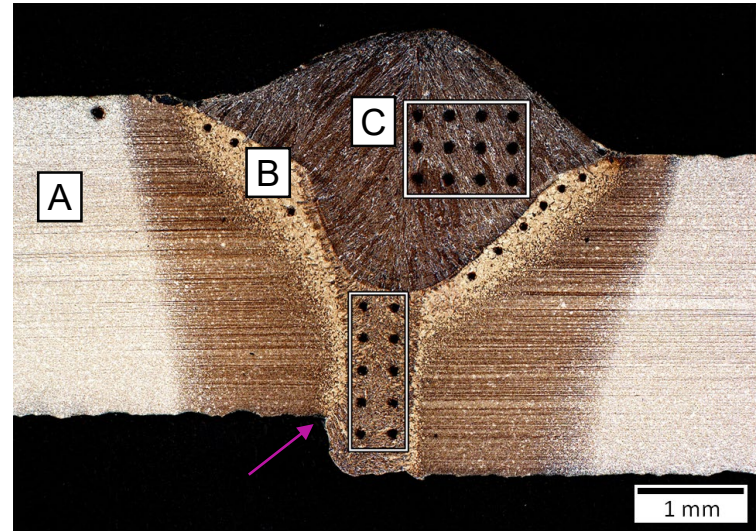
Scope of work

Scope of work

How to predict average strength properties of welded steel from statistical analysis of the microstructure?

Research questions:

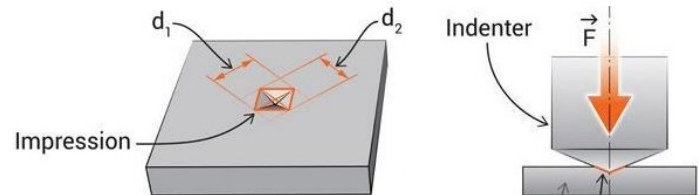
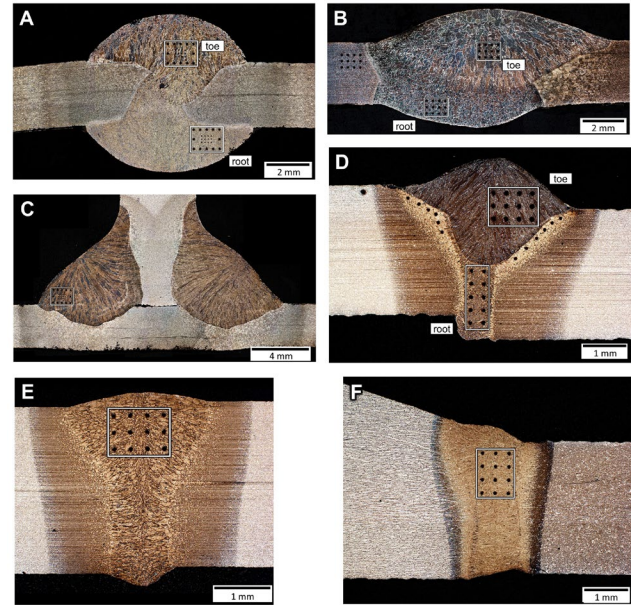
- 1) How to characterize the microstructure
- 2) How to measure local strength variation
- 3) Define dependencies between microstructure and strength



Experiments

Microstructure and strength characterised for several weld metals:

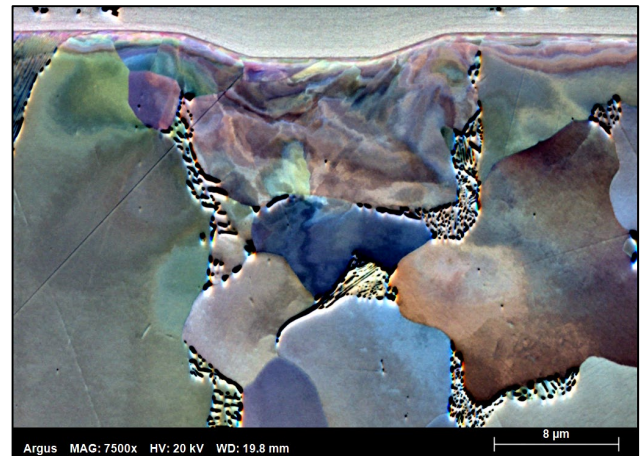
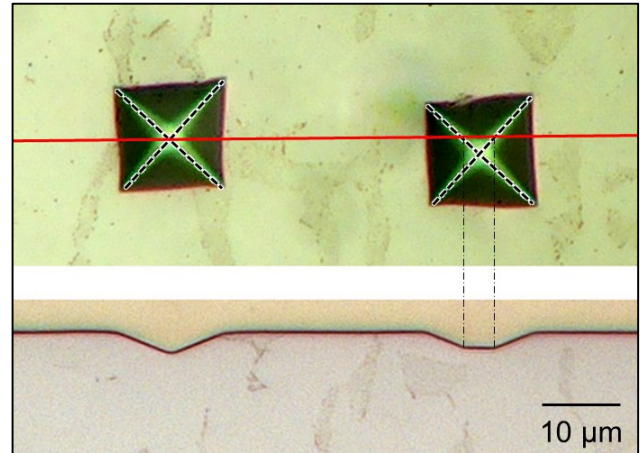
- Instrumented indentation testing to measure local strength properties
- Scanning electron microscopy used for the characterization of microstructure and plastic deformation



Experiments

Microstructure and strength characterised for several weld metals:

- Instrumented indentation testing to measure local strength properties
- **Scanning electron microscopy used for the characterization of microstructure and plastic deformation**

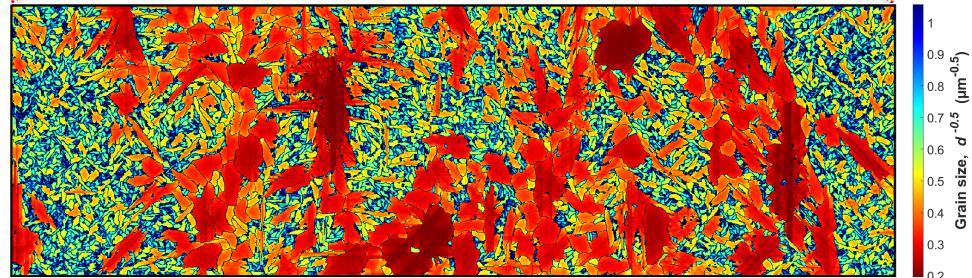
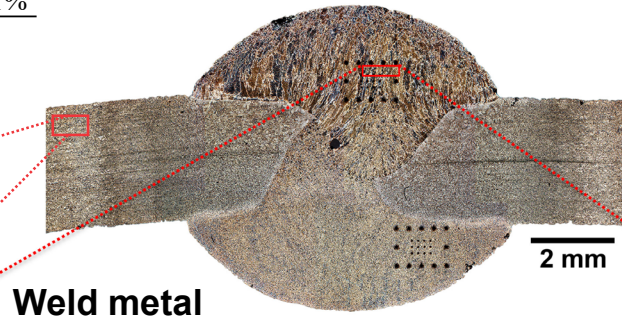
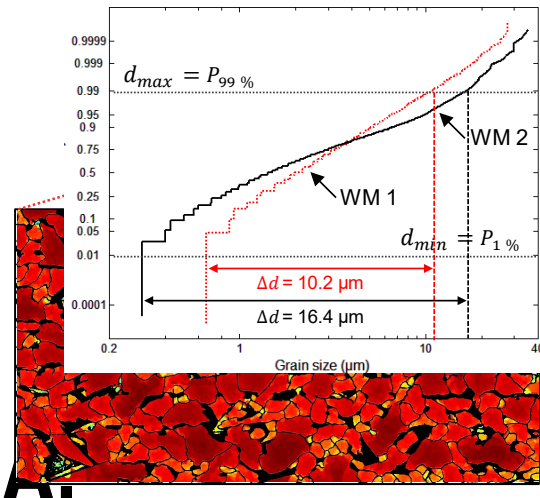


Grain size of steel

- Solidification of a weld creates a broad dispersion of different grain sizes in comparison to base metal
- Methods developed for the characterisation of the heterogeneous grain structure

$$\frac{\Delta d}{d} = \frac{d_{\max} - d_{\min}}{d} = \frac{P_{99\%} - P_{1\%}}{d}$$

Log-normal probability plot



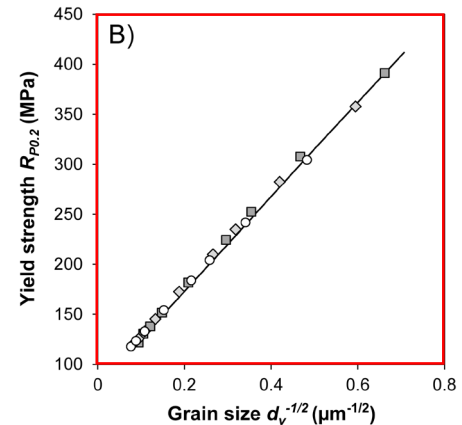
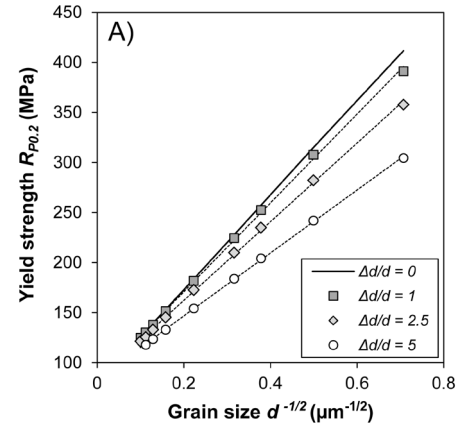
Prediction of strength

- Average strength properties can be predicted using average grain size
- However, the grain size dispersion must be considered
- **Based on the observations of this dissertation, the Hall-Petch equation was modified:**

$$\sigma = \sigma_0 + kd^{-1/2} \left(1 + f \frac{\Delta d}{d} \right)$$

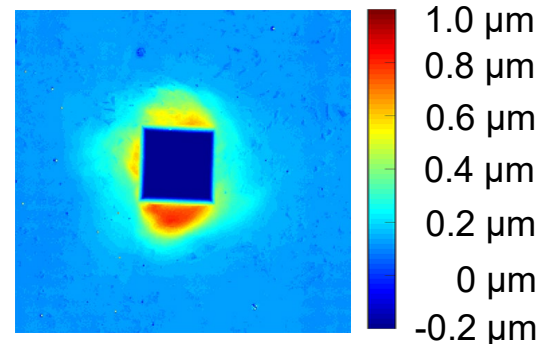
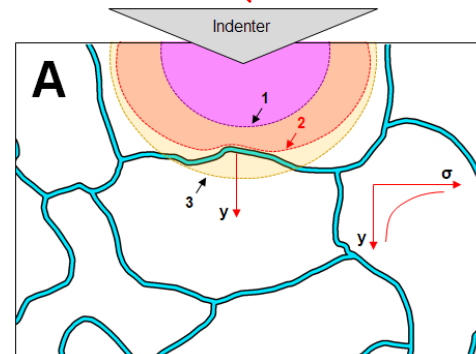
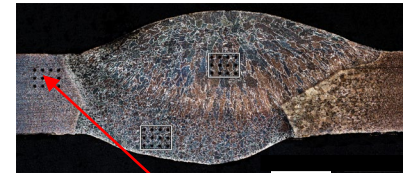
Relative grain size dispersion

Literature: simulated base metal



Local plastic deformation

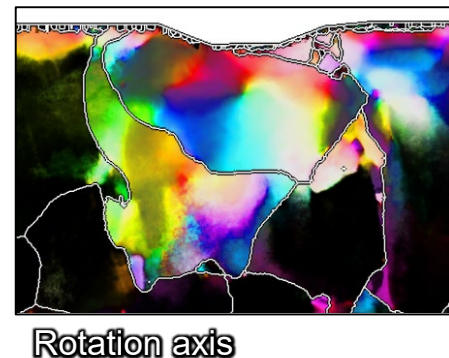
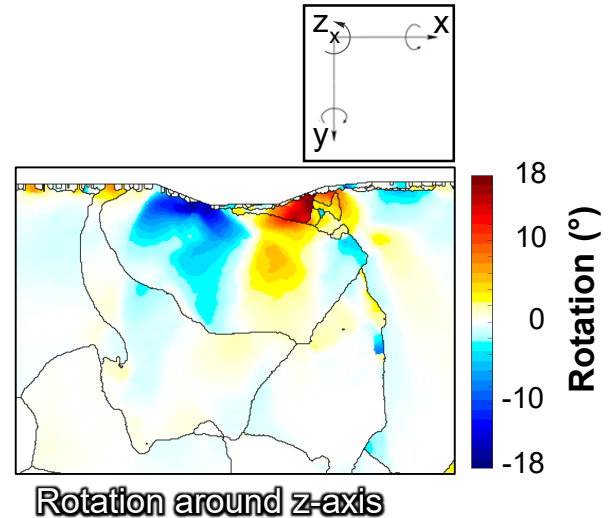
- In a hardness test the material must permanently change its shape to accommodate the indenter
- The mechanism for the shape change is material rotation
- At microstructural level the grains in the material are subdivided into smaller units
- Dislocations are moving on specific slip systems



Indentation depth 4.9 μm

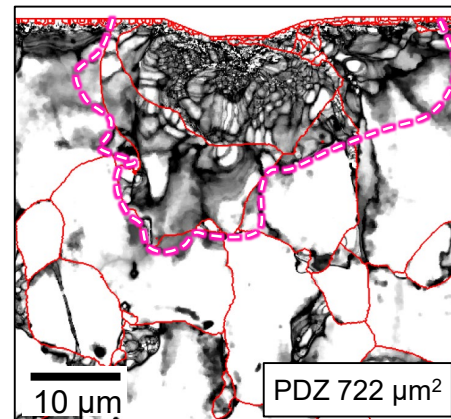
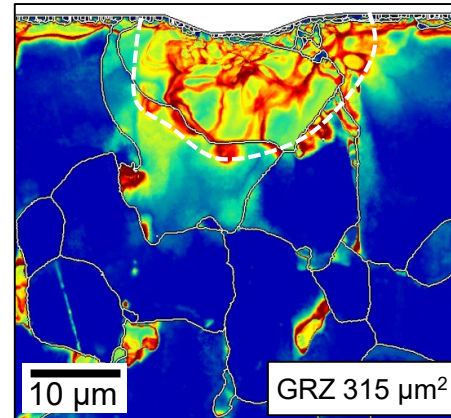
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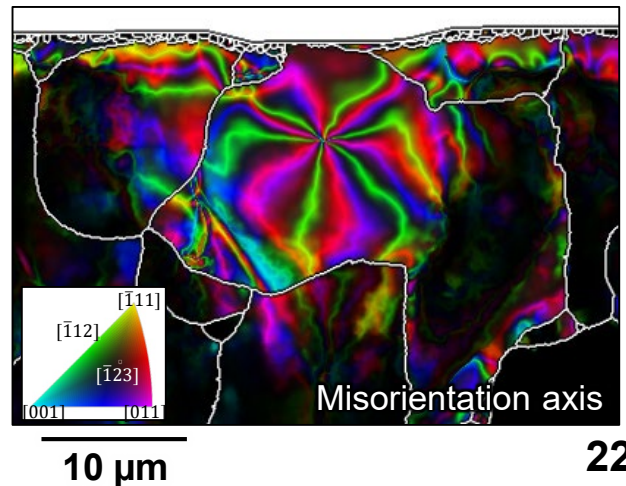
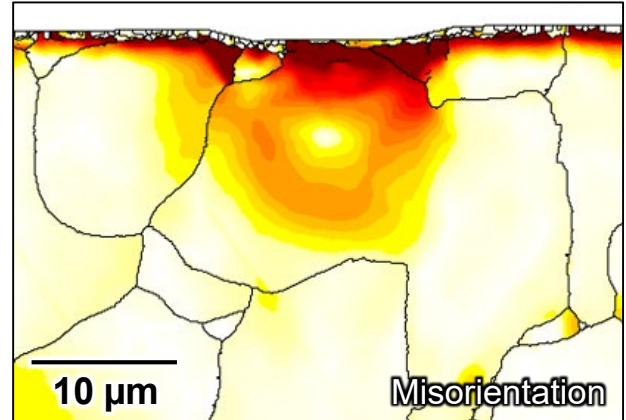
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Local plastic deformation

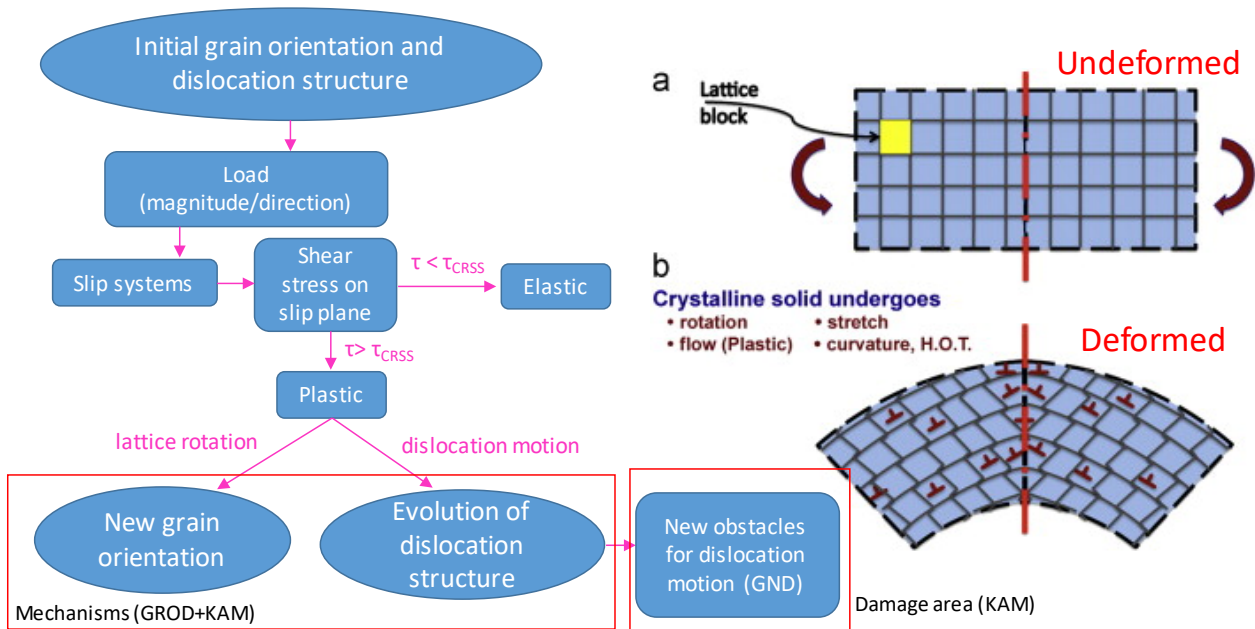
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Local misorientation analysis in MTEX

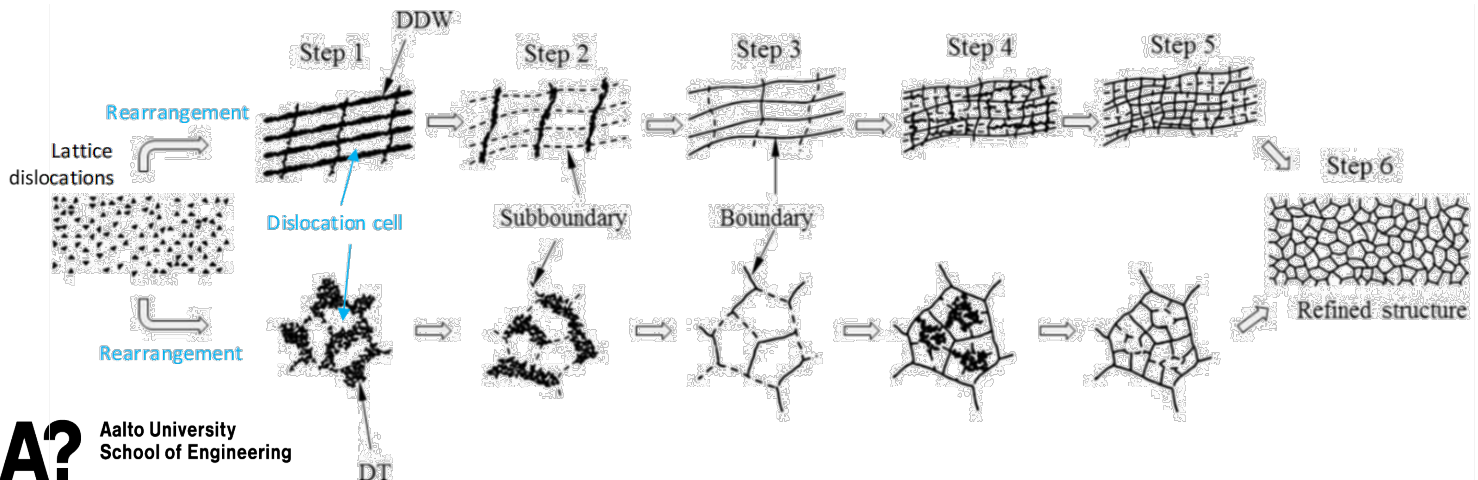
Deformation mechanism of steel

- Two aspects need to be analyzed for local plastic deformation:
 - 1) Changes in grain orientation
 - 2) Evolution of dislocation structure



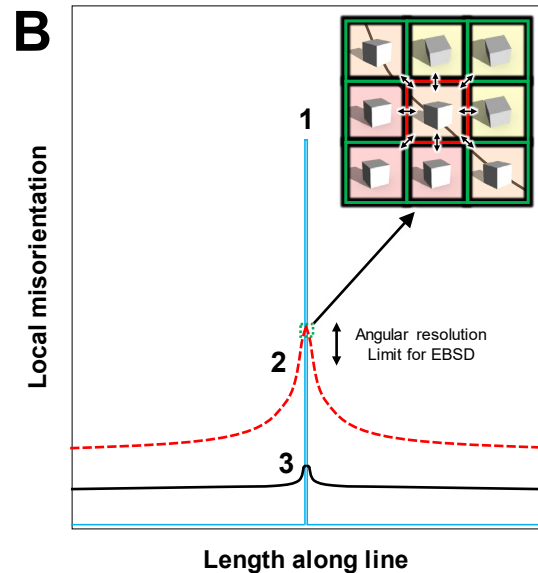
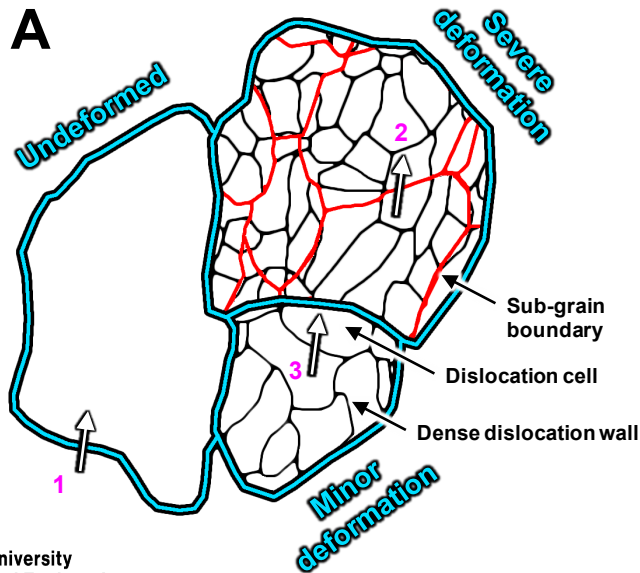
Deformation mechanism of steel

- Grain subdivision process, where lattice dislocations rearrange to form dislocation tangles (DT) and dense dislocation walls (DDW).
- As deformation continues, dislocation density increases, and new sub-grain and grain boundaries are formed.
- With sufficient plastic deformation the process is repeated in the newly formed grains, further refining the grain size.



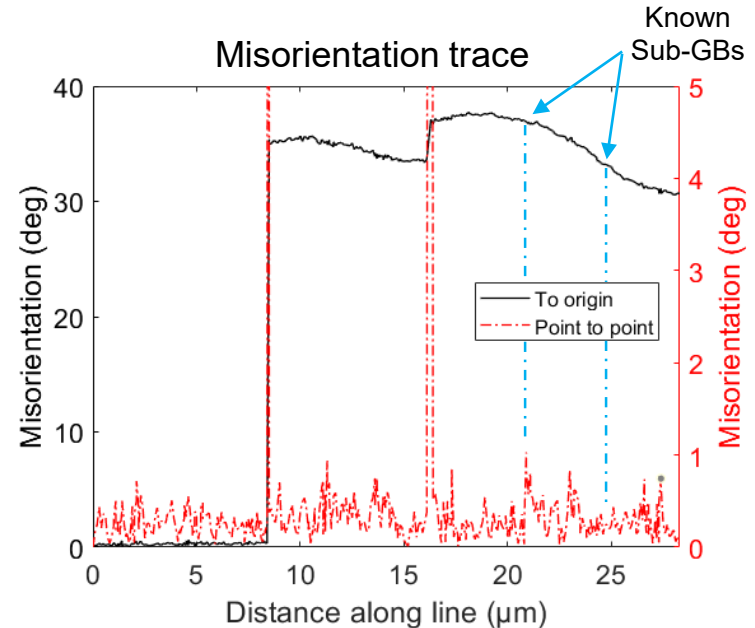
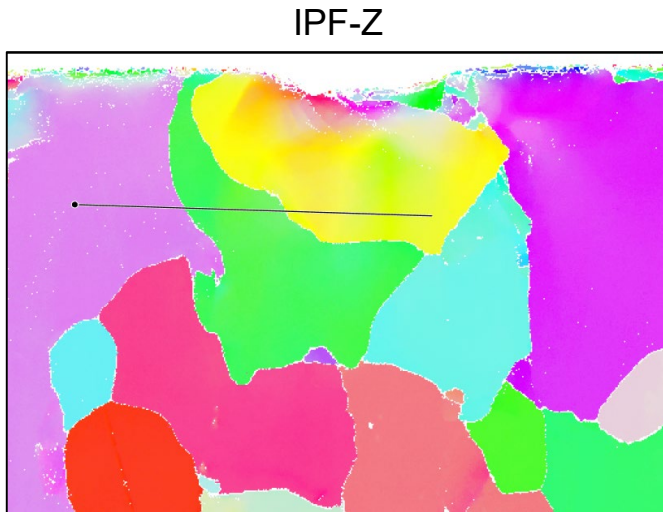
Deformation mechanism of steel

- Sub-grain boundaries are harder to detect than grain boundaries from EBSD data for two reasons:
 - 1. Boundaries are gradual, not sharp
 - 2. Misorientation is small in relation to angular resolution



Deformation mechanism of steel

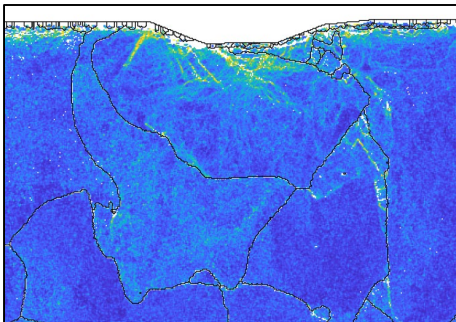
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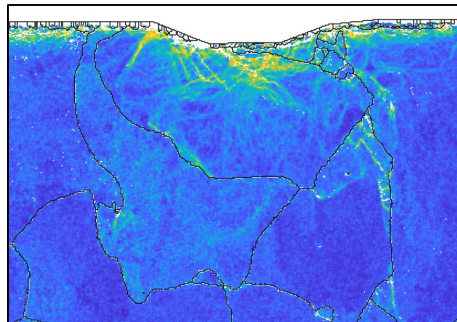
Kernel misorientation

- Kernel misorientation measures the average misorientation between a central point and its nearest neighbours
 - Small kernels affected by the global orientation gradient
 - Some boundaries visible, but the measurement noise inhibits reliable detection of sub-granular features
- => **A new measurement strategy is needed**

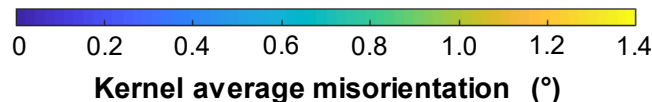
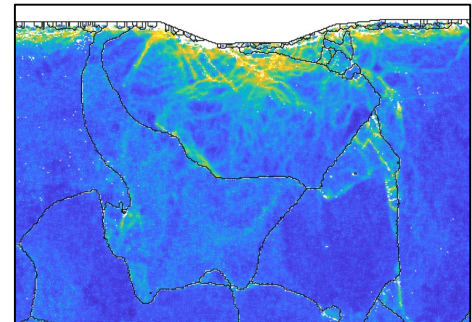
3x3 kernel (nn=1)



5x5 kernel (nn=2)

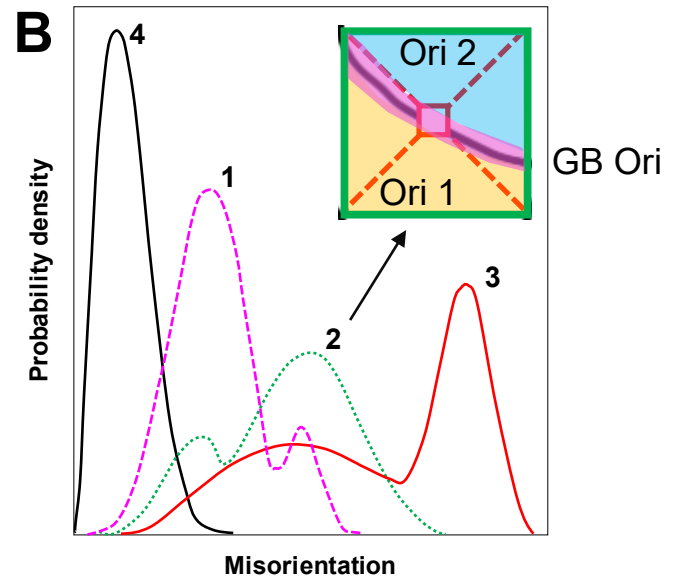
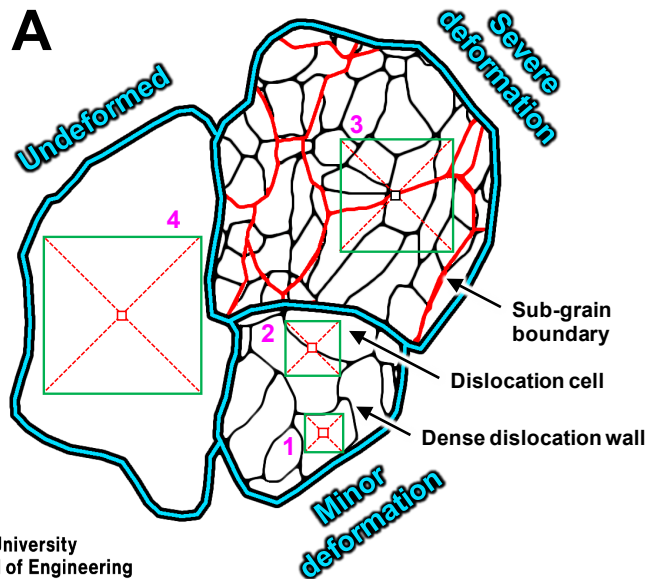


7x7 kernel (nn=3)



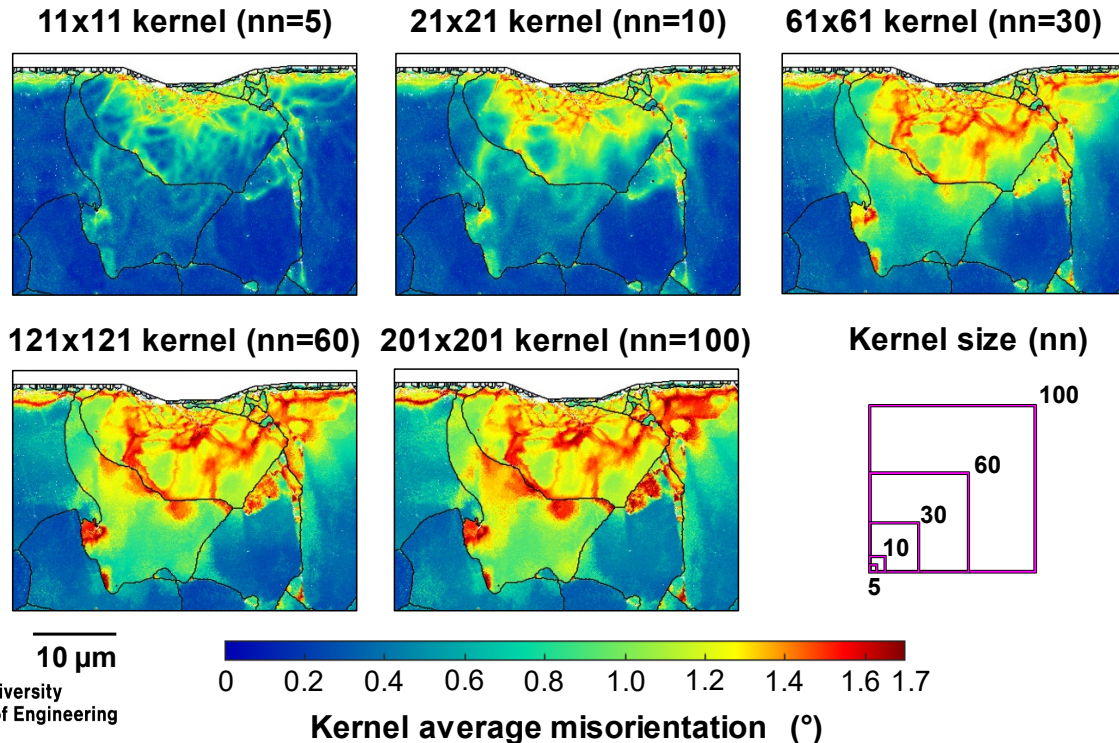
Adaptive kernel size analysis

- Instead of sampling the immediate vicinity of the gradual border, the misorientation between neighbouring sub-grains should be measured
 - Kernel size should be in proportion to the measured sub-granular units
 - Different sub-GB types have characteristic misorientation ranges
 - Large kernels (20..100 nm) effective in averaging EBSD measurement noise



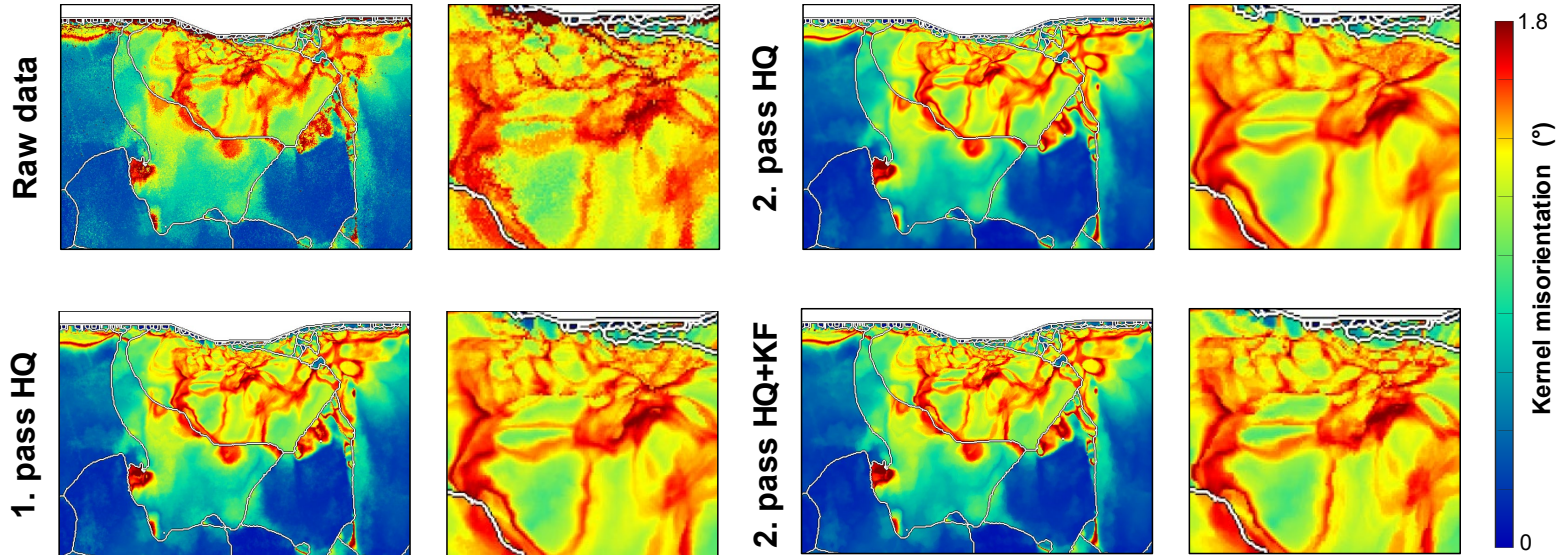
Adaptive kernel size analysis

- Kernel size up to 100 nearest neighbours (0.1 μm step size)
- Misorientation analysis range 0 – 2° reveals sub-grain boundaries
- Large kernels minimise the effect of global orientation gradient



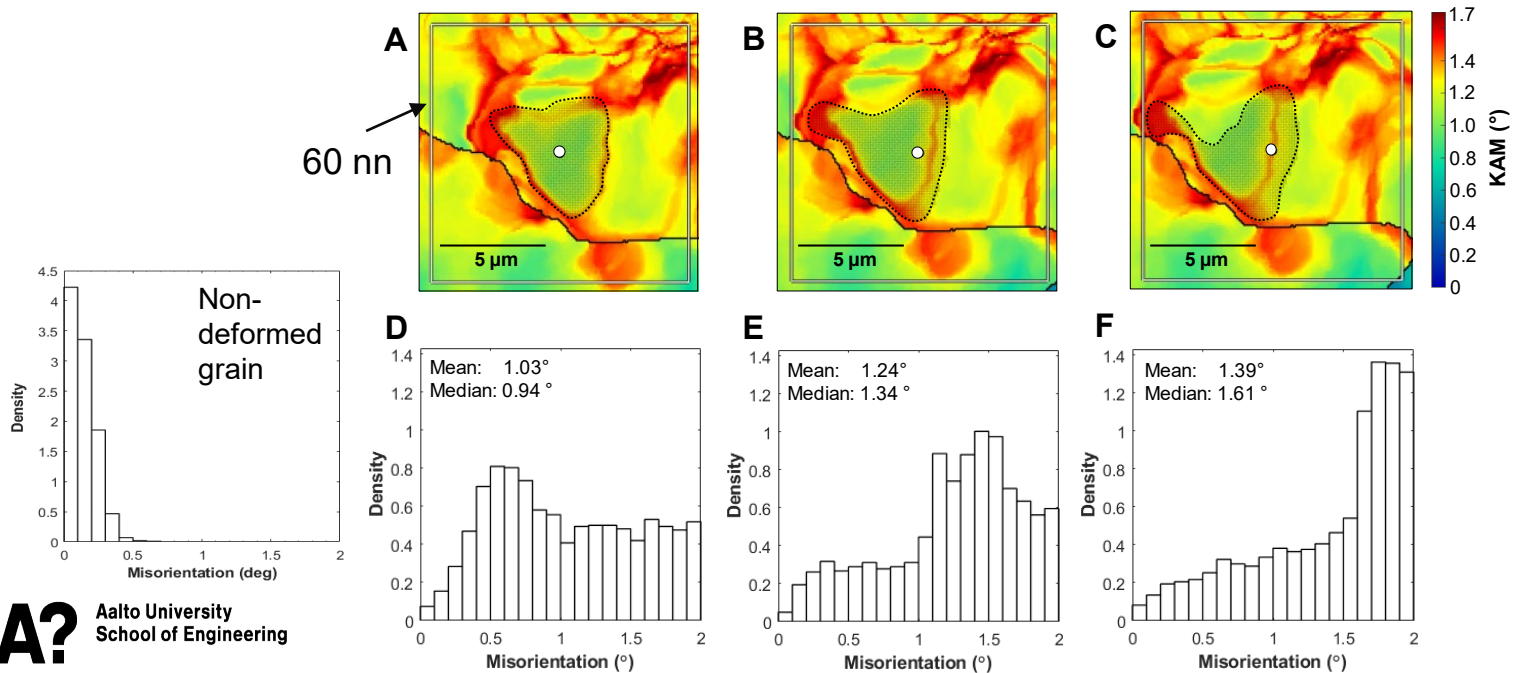
Post-processing of EBSD data

- Noise of EBSD data can be effectively reduced with MTEX to enhance visibility of sub-granular features
- Combination of Half-Quadratic filter ($\alpha=0.15$) and Kuwahara Filter (1st NN) suitable for reducing measurement noise while retaining sub-granular detail (MTEX 5.0.1)



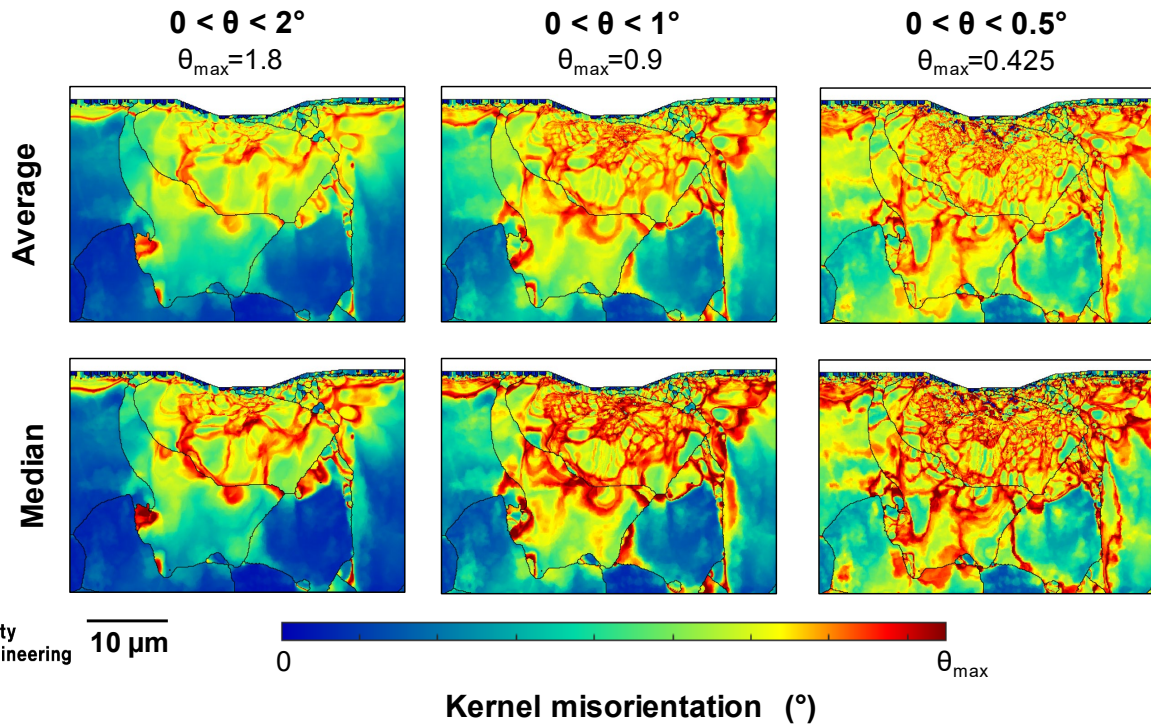
Effective kernel size

- The effective kernel size is dependent on size of features and location of measurement point
- In the example below, 60 nm kernel is moved inside a sub-grain



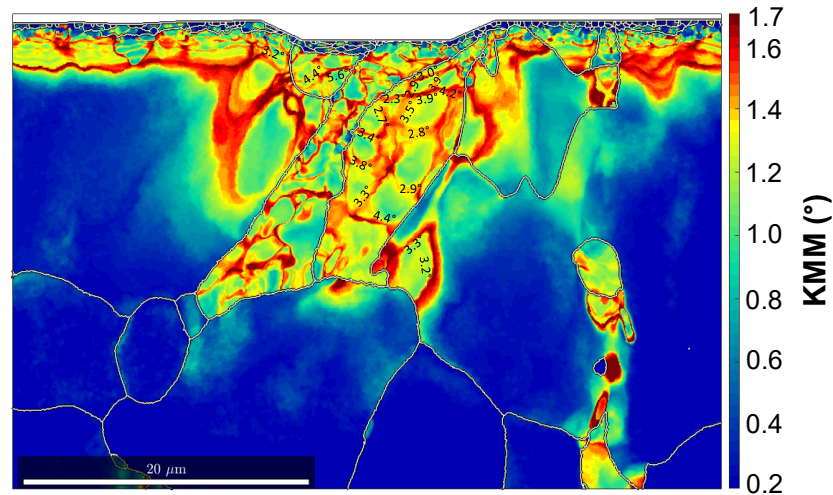
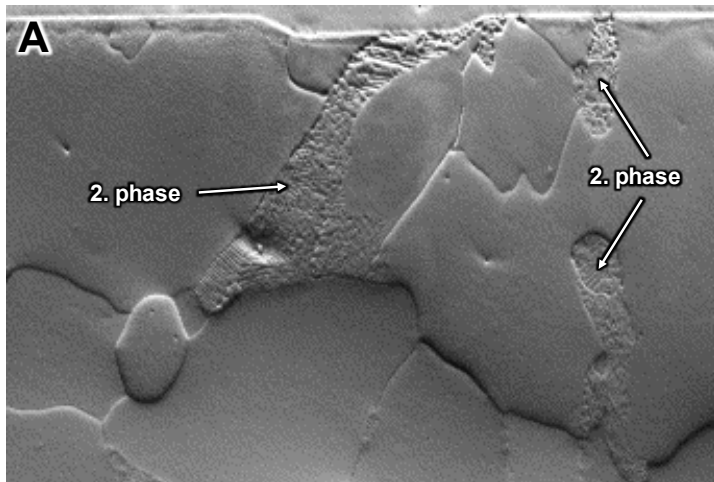
Sub-grains and dense dislocation walls

- By analyzing smaller misorientation ranges, the dense dislocation walls become visible
- Median value enhances contrast between non-deformed and deformed areas for 0-2° range



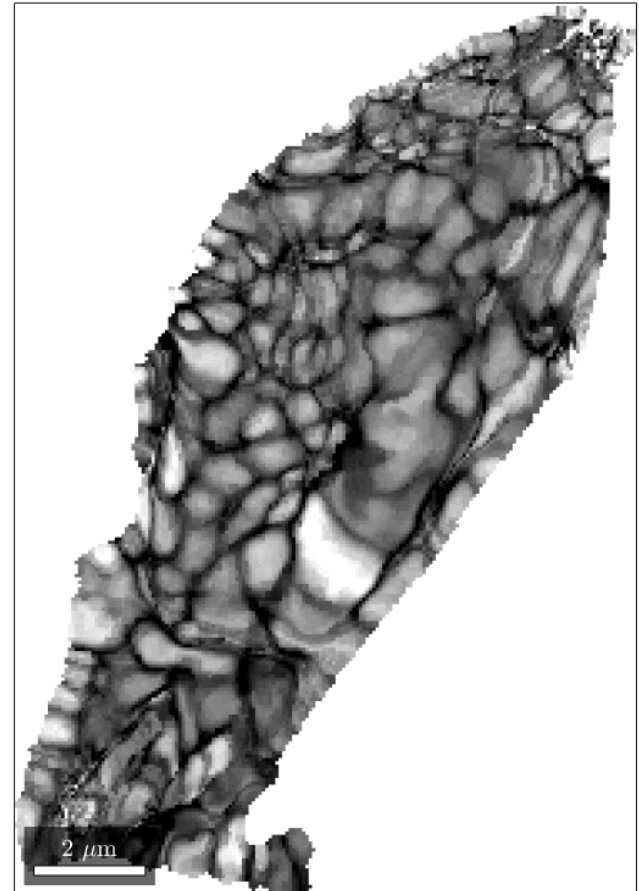
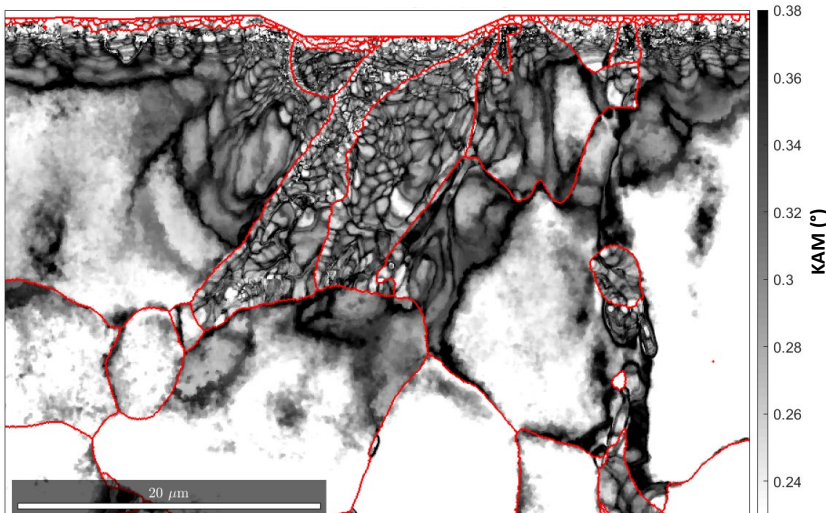
Sub-grains and dense dislocation walls

- Misorientation between neighbouring sub-grains 2.3 – 5.6°, average 3.5°



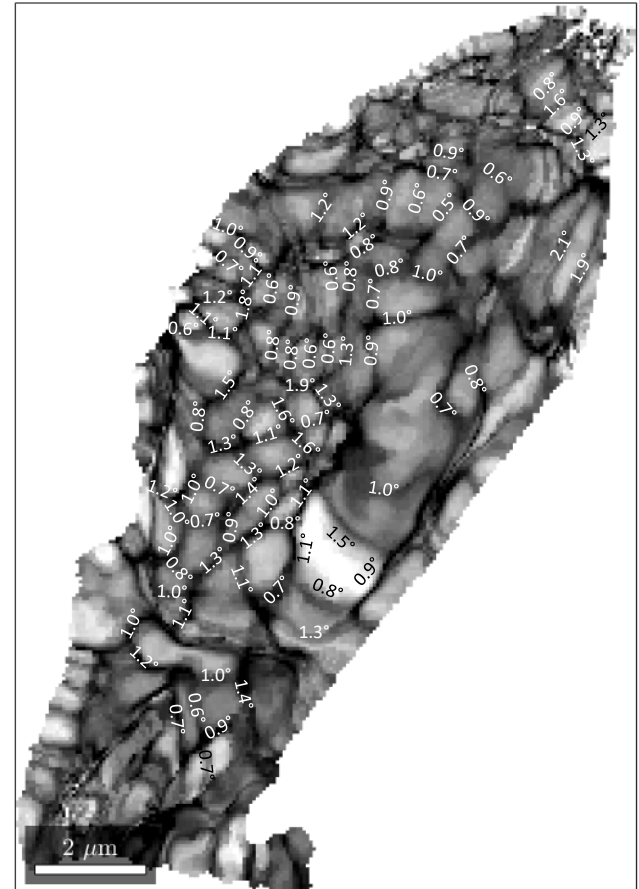
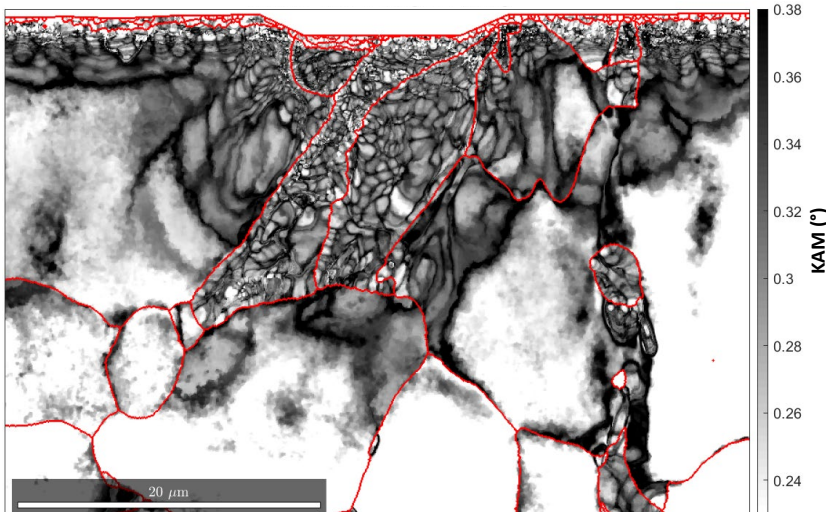
Sub-grains and dense dislocation walls

- Misorientation between neighbouring dislocation cells $0.5 - 2.1^\circ$, average 1.0°



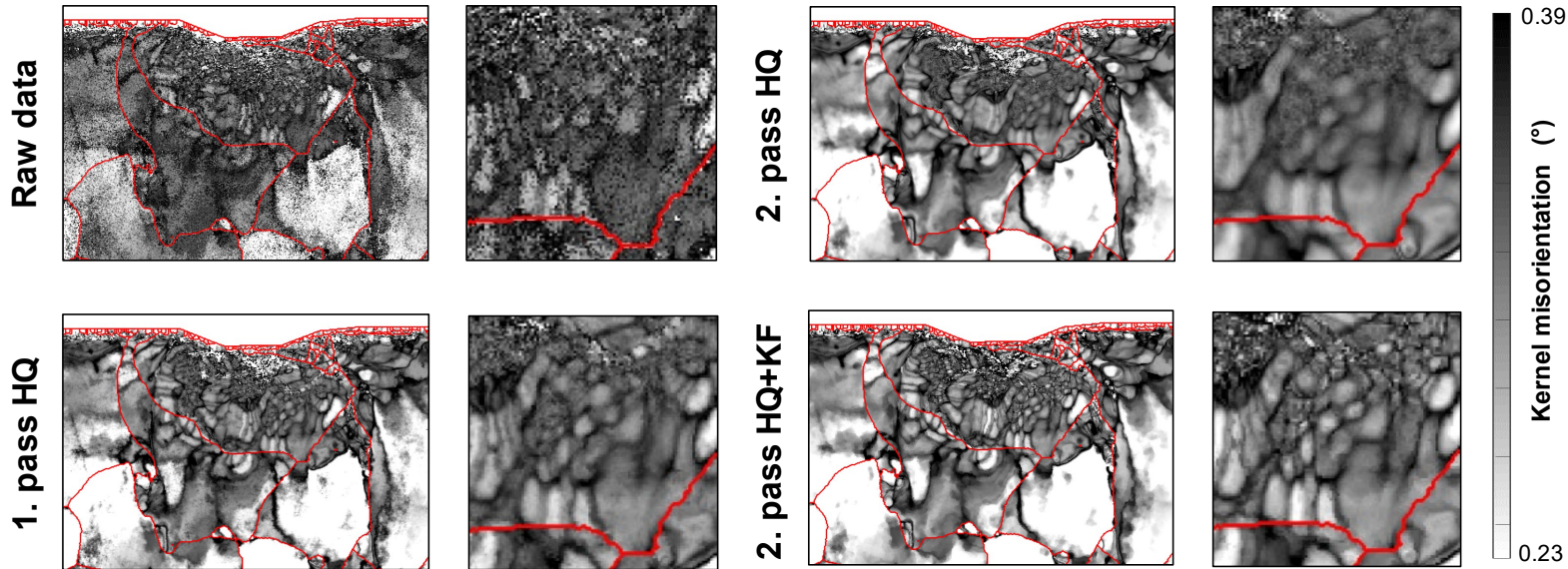
Sub-grains and dense dislocation walls

- Misorientation between neighbouring dislocation cells $0.5 - 2.1^\circ$, average 1.0°



Post-processing of EBSD data

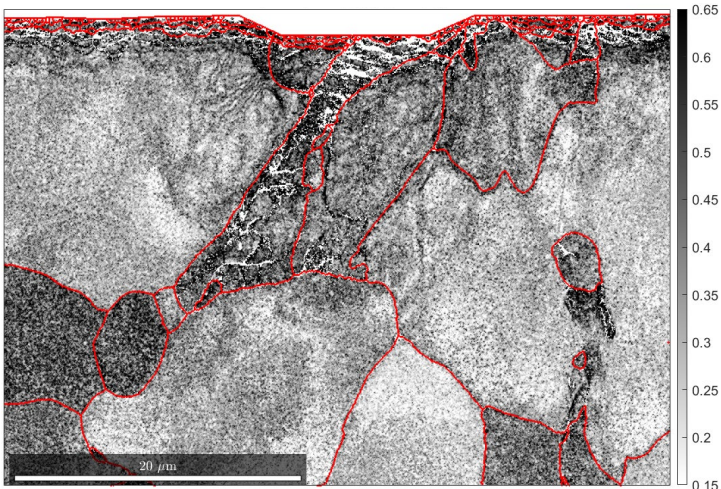
- Combination of Half-Quadratic filter ($\alpha=0.15$) and Kuwahara Filter (1st NN) suitable for reducing measurement noise while retaining dislocation cell detail (MTEX 5.0.1)



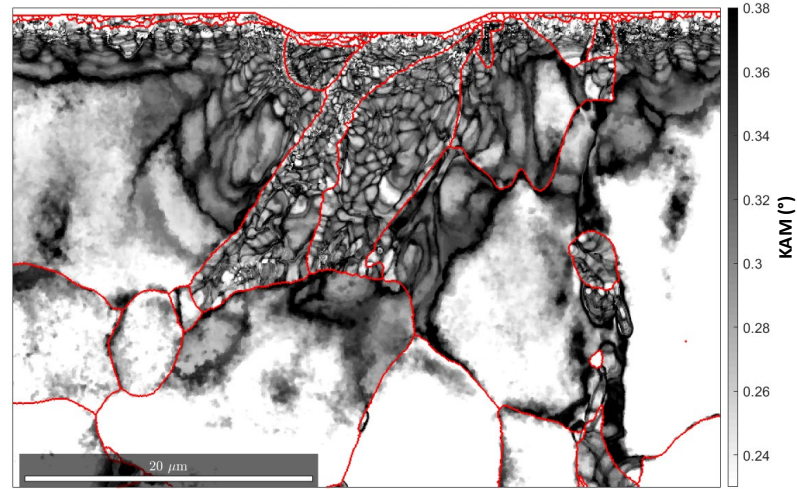
Post-processing of EBSD data

- Comparison of detail resolved with 0.06 μm step size:
 - Raw data and conventional KAM
 - Post-processed data and adaptive kernel size approach

Conventional KAM 1 nn & Raw data

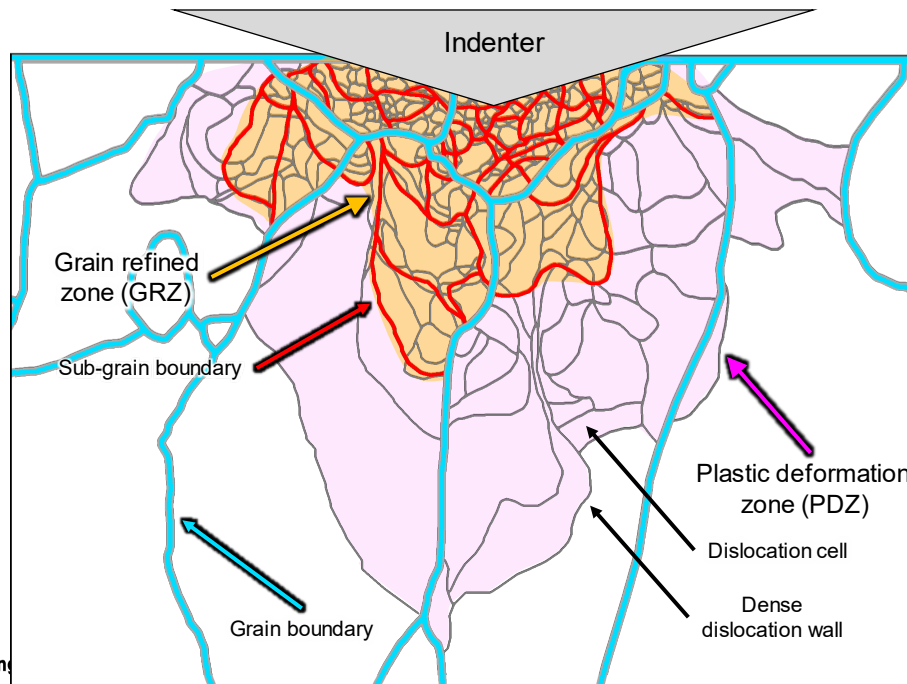


Kernel size: 100 nn & 2. Pass HQ + KF 1



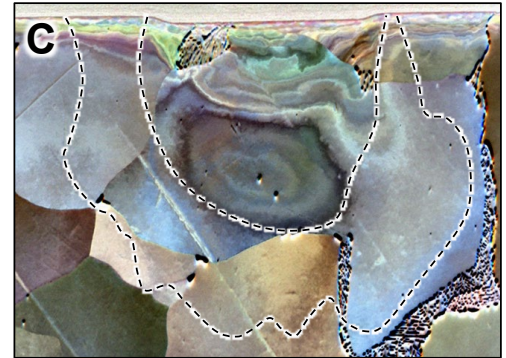
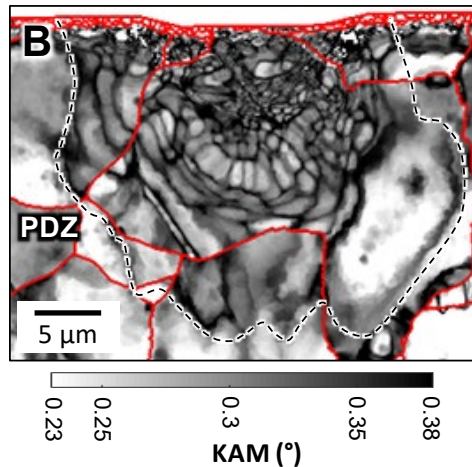
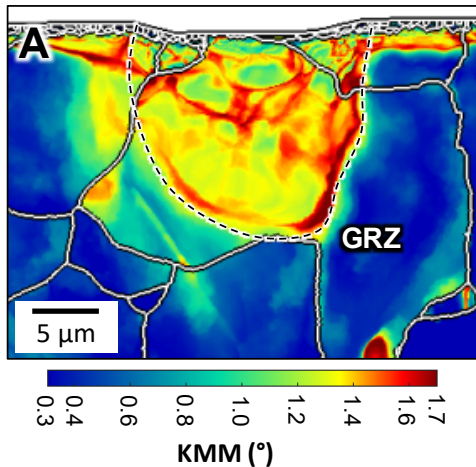
Plastic deformation zone

- Two deformation zones can be defined:
 - 1) Grain refined zone with sub-grain boundaries (KMM 0-2°)
 - 2) Plastic deformation zone with dense dislocation walls (KAM 0-0.5°)



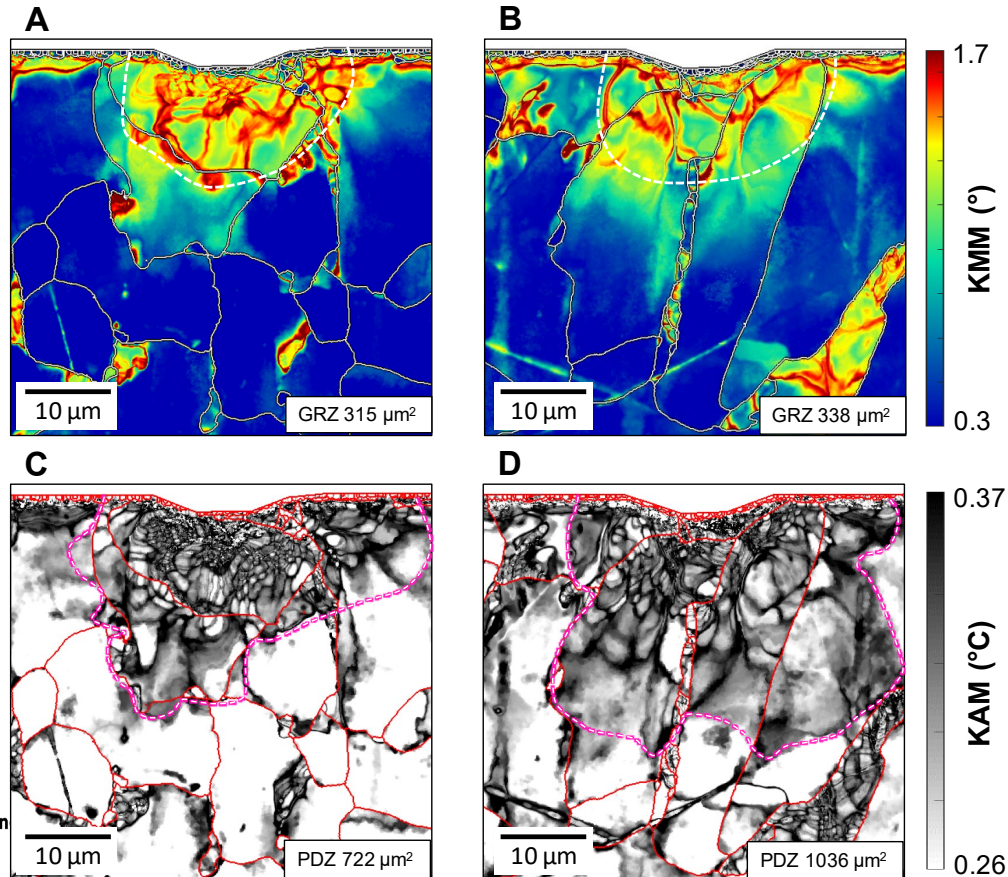
Plastic deformation zone

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Plastic deformation zone

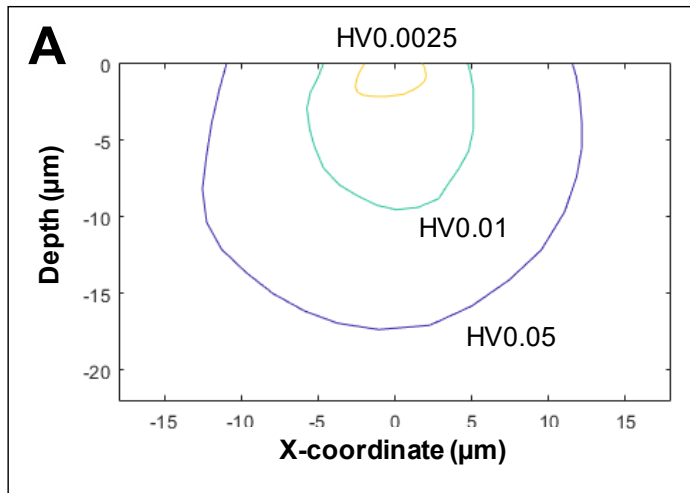
- Influence of grain boundaries and grain size on deformation can be analysed



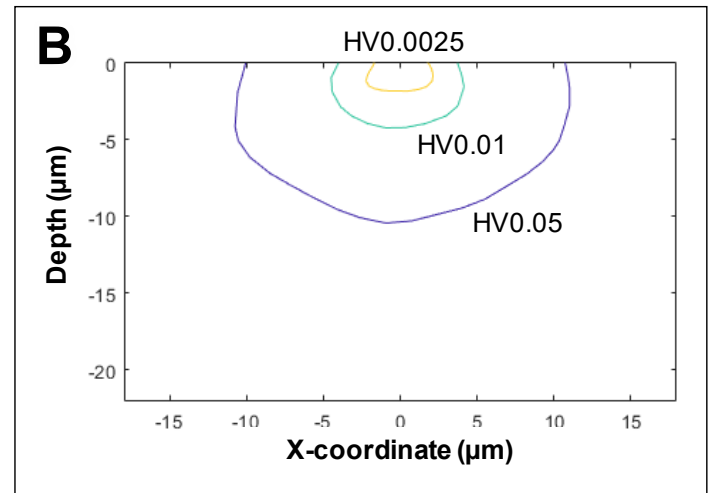
Plastic deformation zone

- Average shape of grain refined zone for two materials at different indentation load levels

Base metal S355

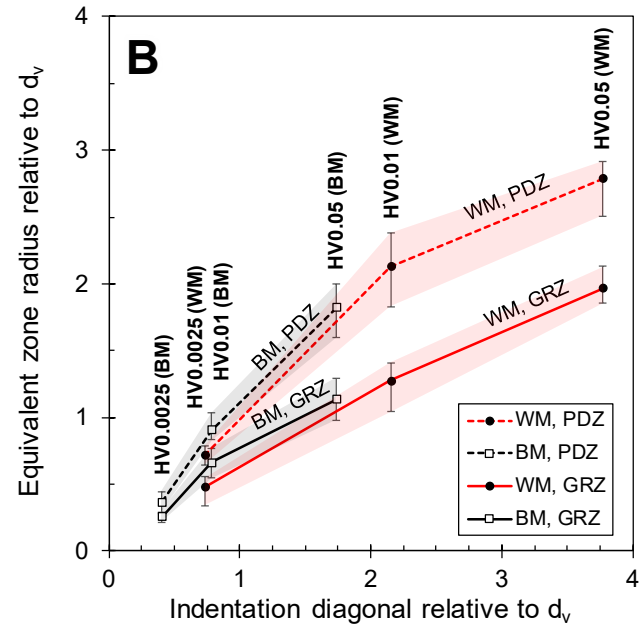
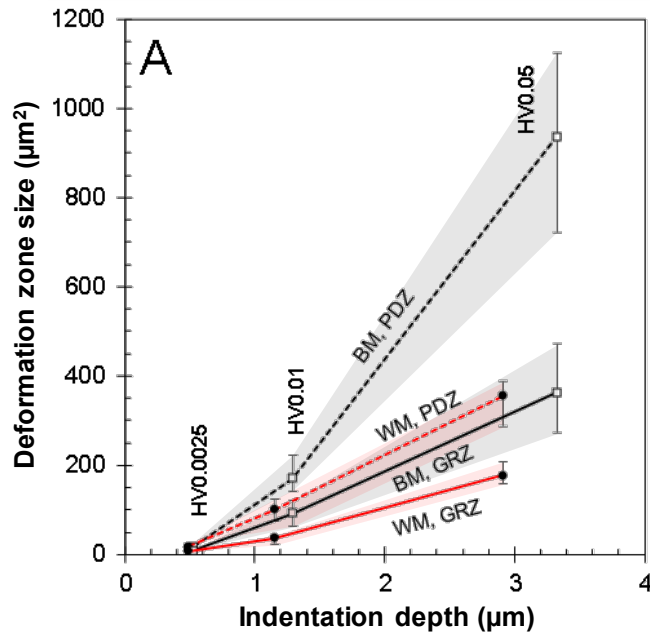


Weld metal



Plastic deformation zone

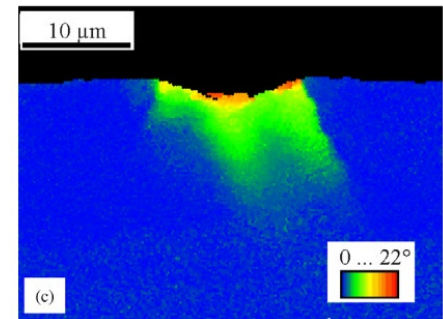
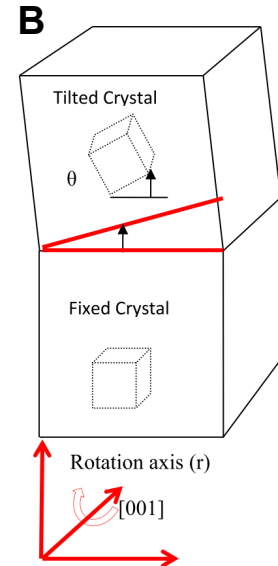
- Average plastic deformation zone can be related to grain size
- Normalisation of deformation zone radius and indentation diagonal with volume-weighted average grain size



Lattice rotation analysis in MTEX

Lattice rotation analysis

- Deformation inside a grain can be measured by comparing the orientations inside a grain to a pre-defined reference orientation
 - Grain reference orientation deviation (GROD) or in MTEX `mis2mean`
- Angle – axis pair
- Accurate definition of reference important, but challenging for polycrystalline materials



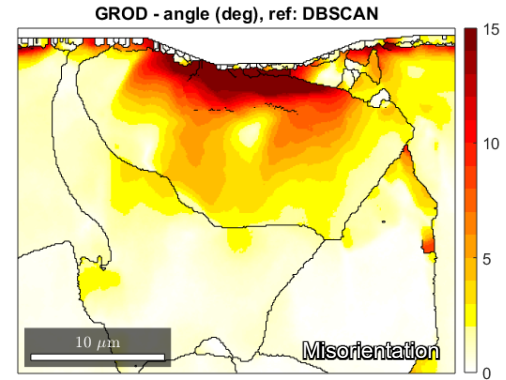
Lattice rotation analysis

From single crystal to polycrystalline material:

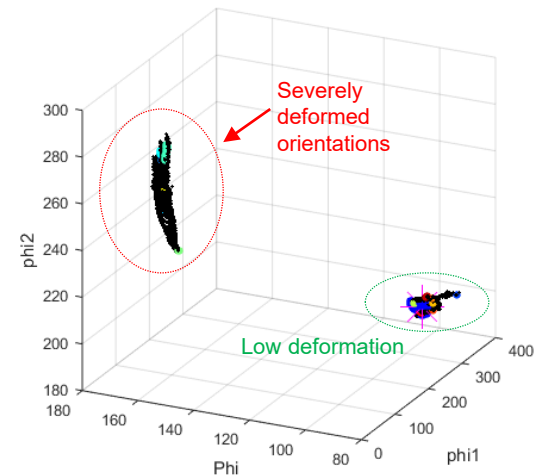
- Grain orientation not known before testing

Level of deformation inside the grain can be severe: how to determine reference orientation?

- Average orientation of the grain
 - Suitable only when level of deformation is low and limited to a small area inside the grain
- Point with the highest pattern quality
 - Assumption that pattern quality correlates with plastic deformation.
 - However, pattern quality is affected by a number of other factors, making this approach unreliable.
- Point with the lowest local misorientation
 - Local misorientation also correlates with plastic deformation.
 - Reference determination unreliable, as the single orientation can deviate significantly from other points with low local misorientation



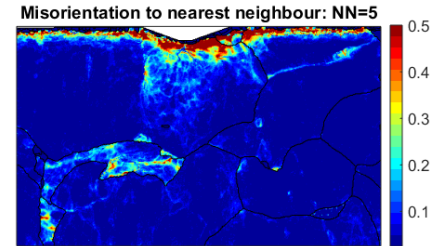
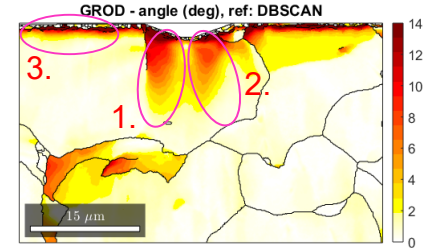
Orientation Euler angles



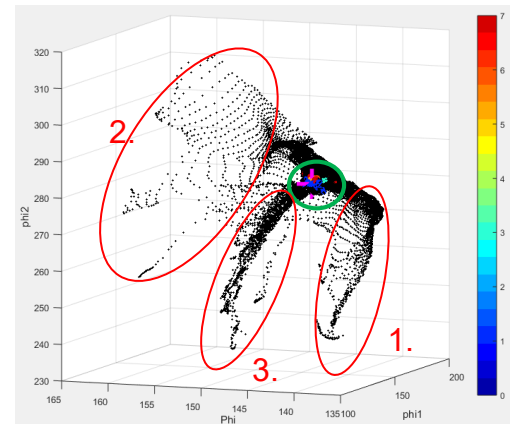
Clustering based reference orientation

- Deformation causes orientation gradients: large misorientation to the closest neighbour inside the grain
- Undeformed areas have similar orientation, causing the misorientation to the nearest neighbour to be very small; **In the example case ~45% of all orientation in the grain are in close proximity to each other**

=> Orientations can be grouped with a density based clustering algorithm DBSCAN

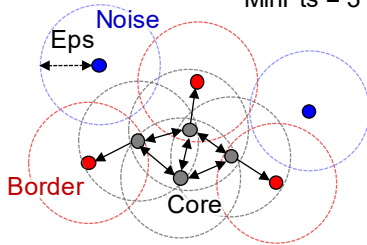


Orientation distribution inside the grain



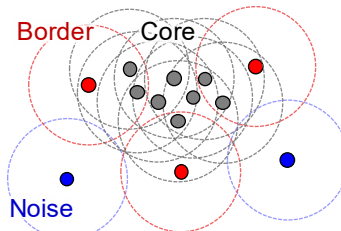
A) Low-density cluster

MinPts = 3



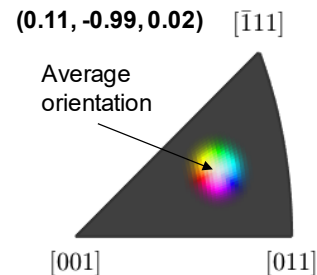
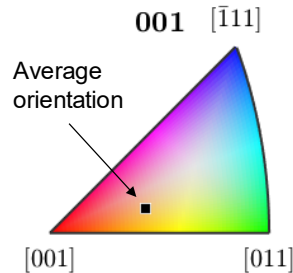
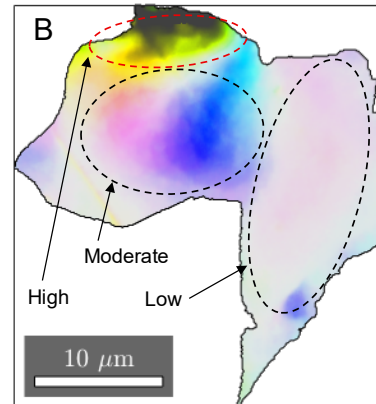
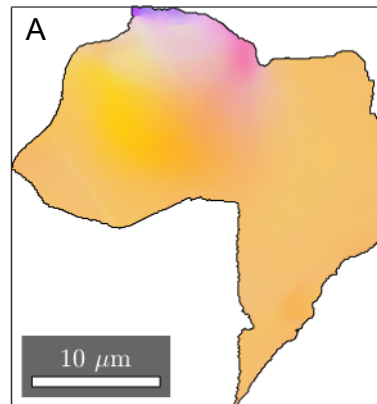
B) High-density cluster

MinPts = 3



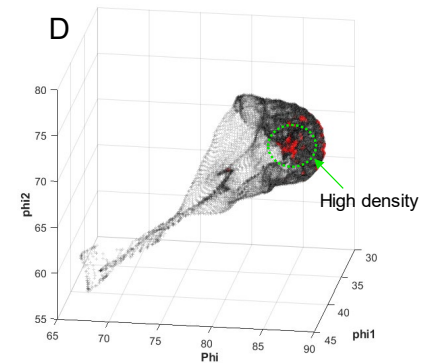
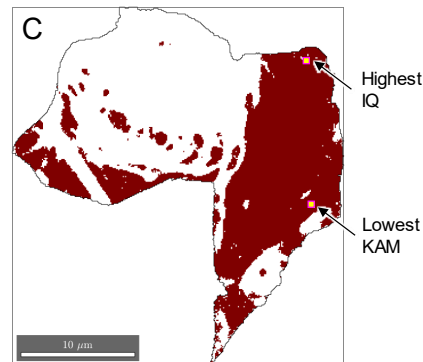
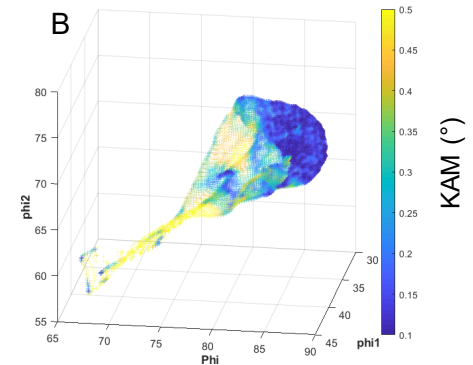
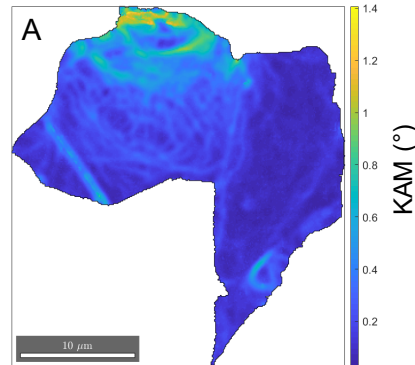
Clustering based reference orientation

- Instead of using all grain orientations, the areas with low deformation should be used



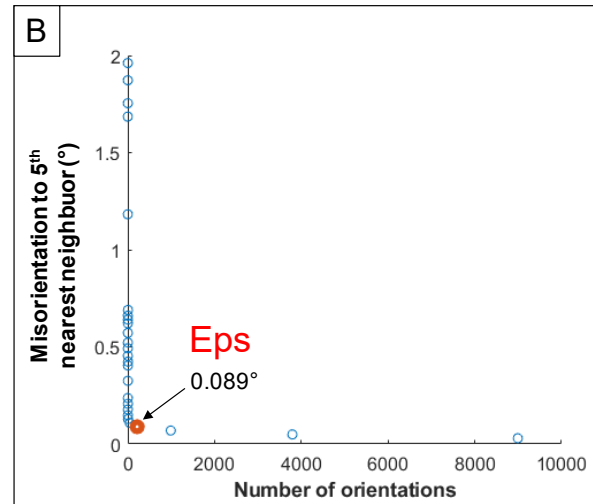
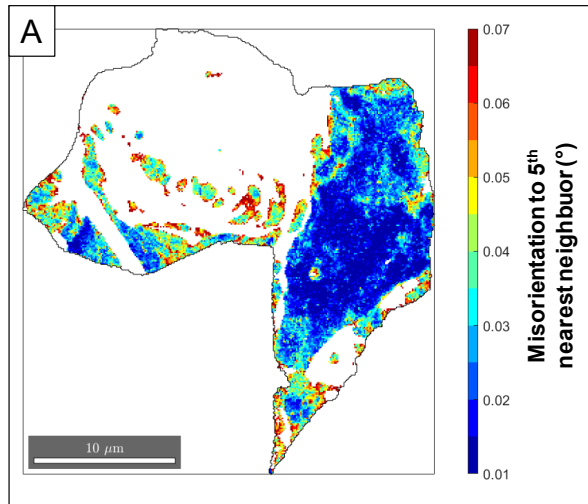
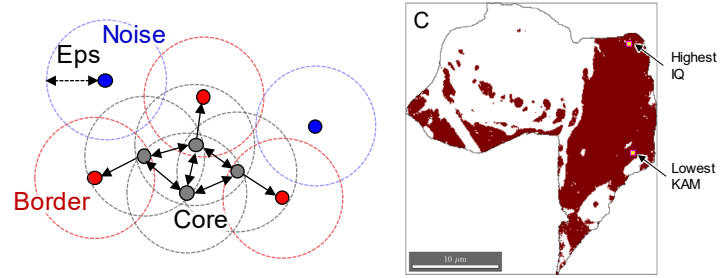
Clustering based reference orientation

- A-B) Kernel misorientation used to determine plastic deformation inside the grain (5th nn)
- C-D) 50% of Lowest KAM are used for clustering, and this already leaves out most of the deformation
- While using a fixed percentage of low KAM areas is feasible, automating the correct value is difficult (grain size, level of deformation)
- => Clustering used to group similar orientations



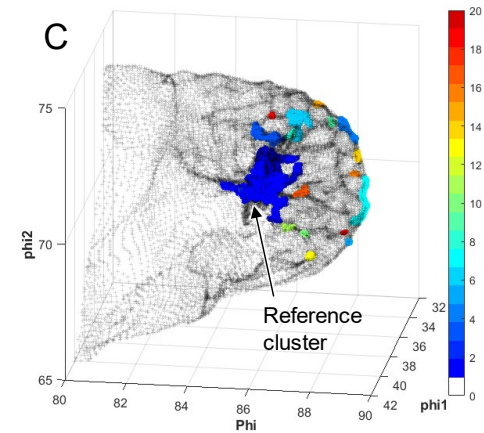
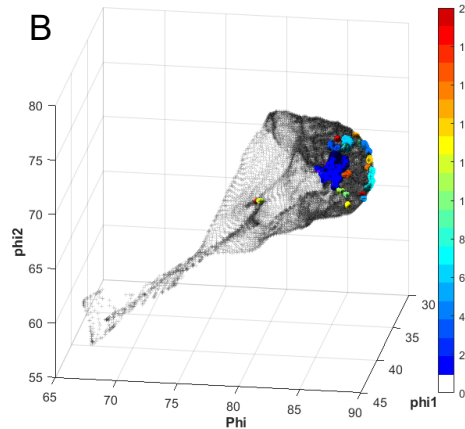
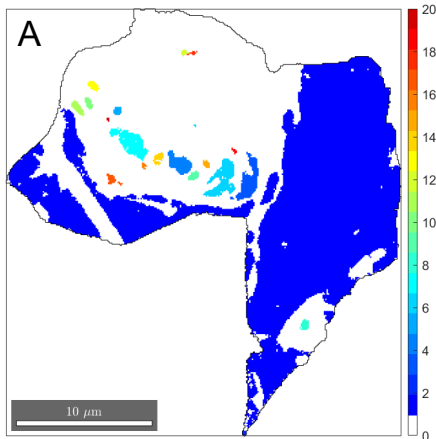
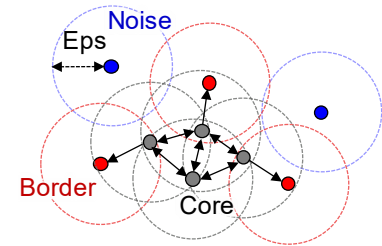
Clustering based reference orientation

- An algorithm is required to determine the clustering parameter 'Epsilon'
- Done individually for each grain, (A) shows the misorientation to 5th nearest neighbour (no spatial information)
- In (B) the knee-point defined with bi-linear fitting defines the clustering parameter



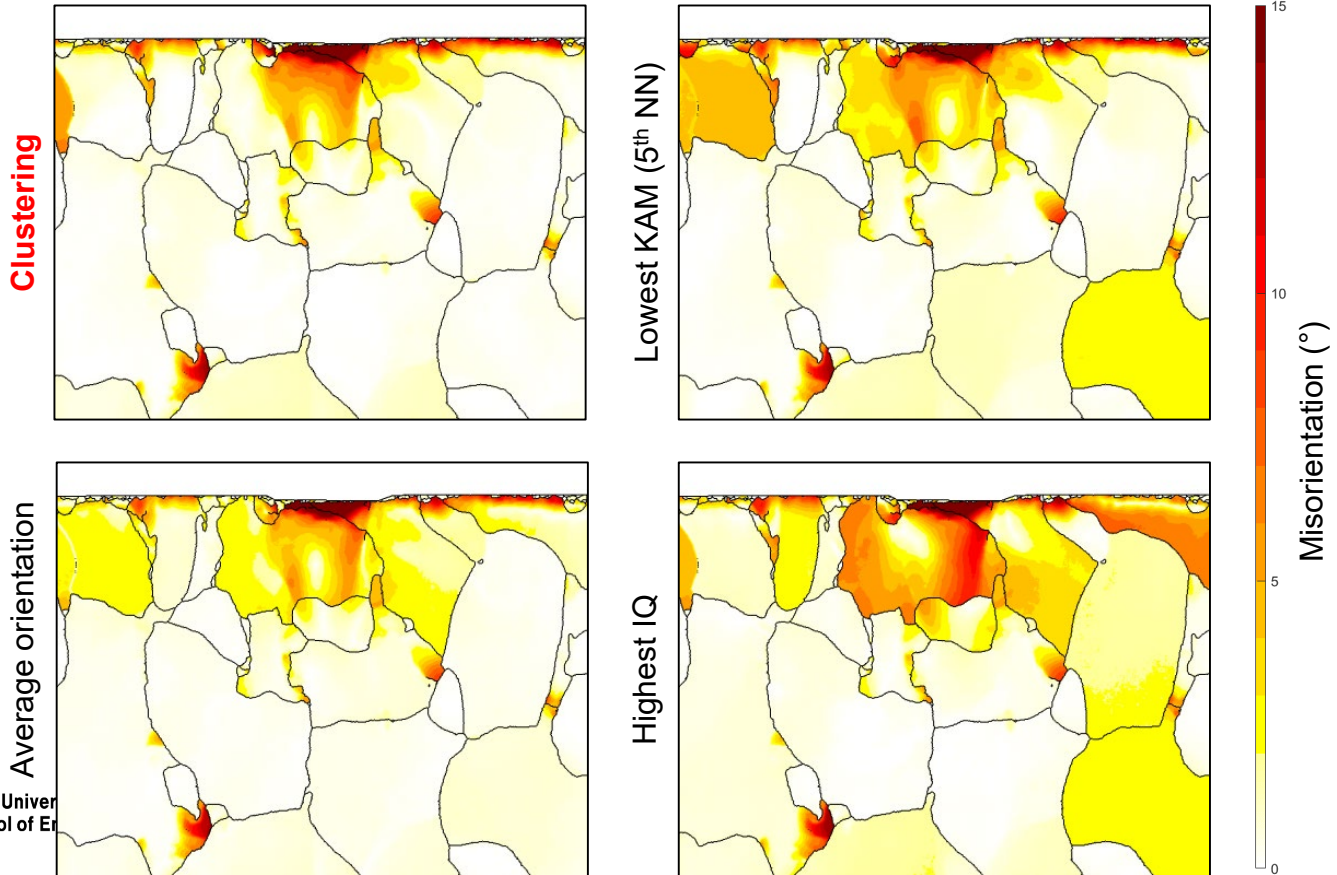
Clustering based reference orientation

- Clustering parameters: Eps= 0.089° , MinPTS = 5
- One large cluster with large density, 19 small clusters
- **Reference orientation is the median of the largest cluster**
 - Flexibility to manually choose other clusters, or to re-run clustering with alternative parameters for selected grains



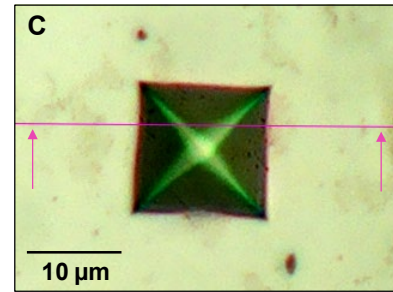
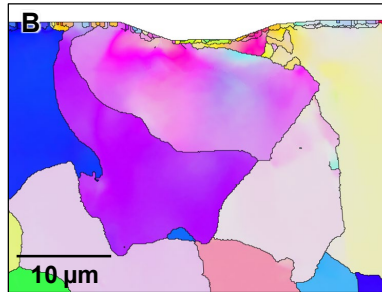
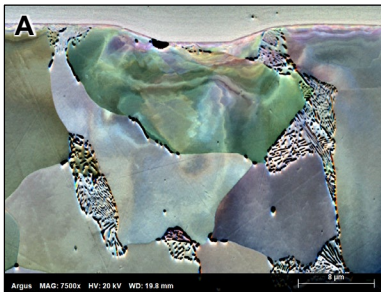
Clustering based reference orientation

- Example of misorientation with different reference orientations



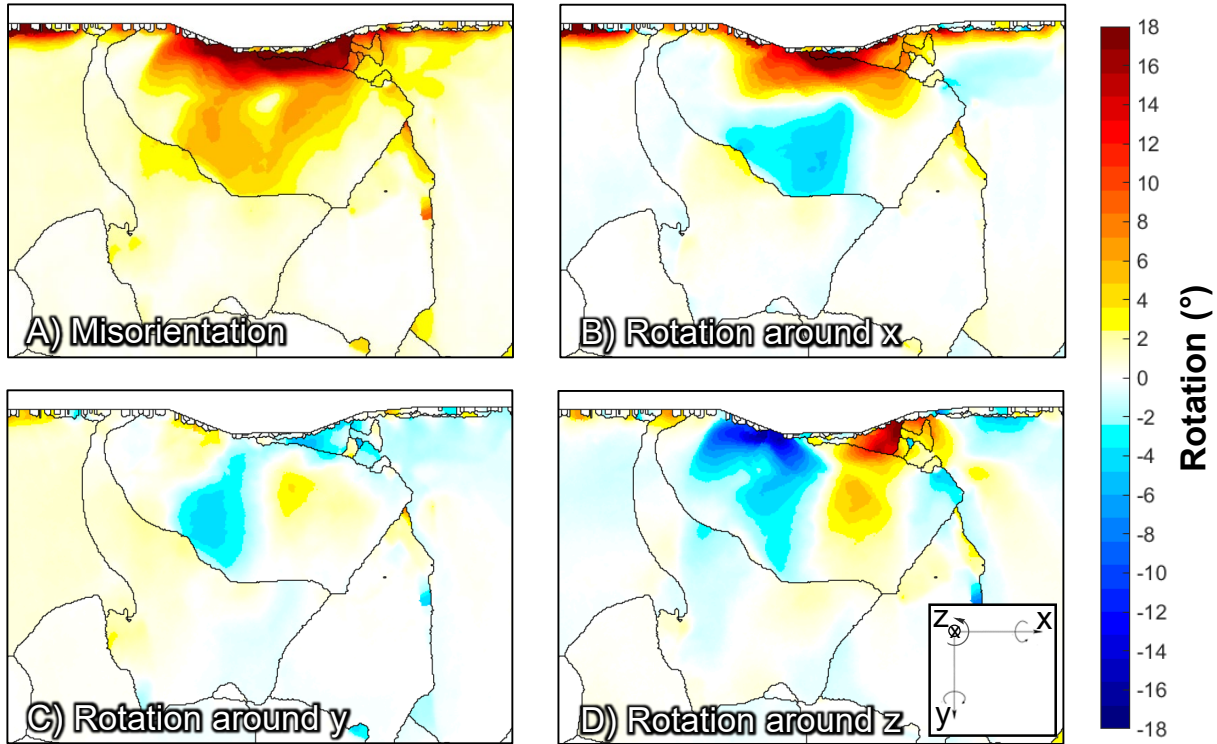
Misorientation analysis

- Example case with S355 structural steel and HV0.05 indentation to demonstrate misorientation analysis with clustering based reference orientation
- For misorientation analysis the Kuwahara Filter is not recommended, often 1. pass of Half-Quadratic filter is enough (in some cases 2. passes)



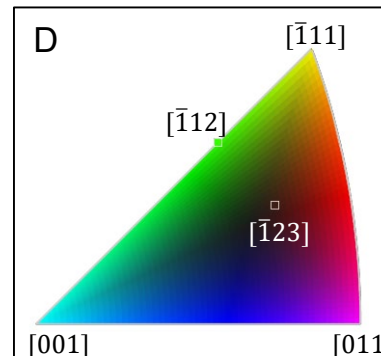
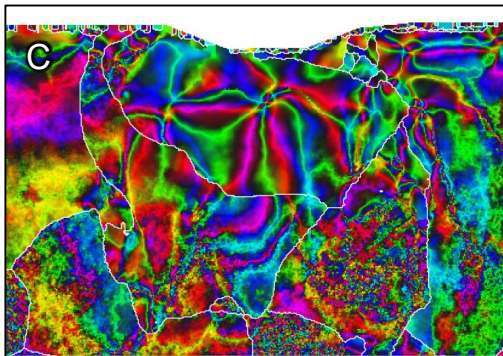
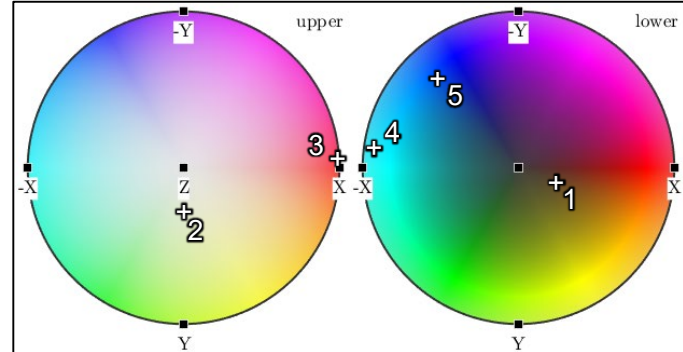
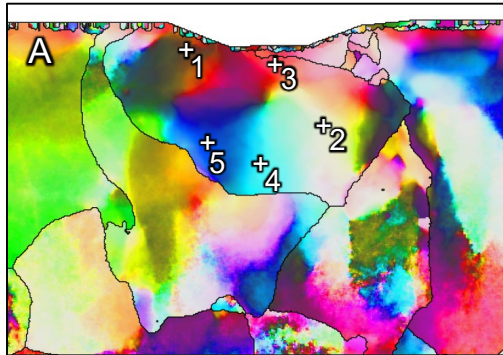
Misorientation analysis

- Misorientation angle, and rotation relative to the specimen coordinate system



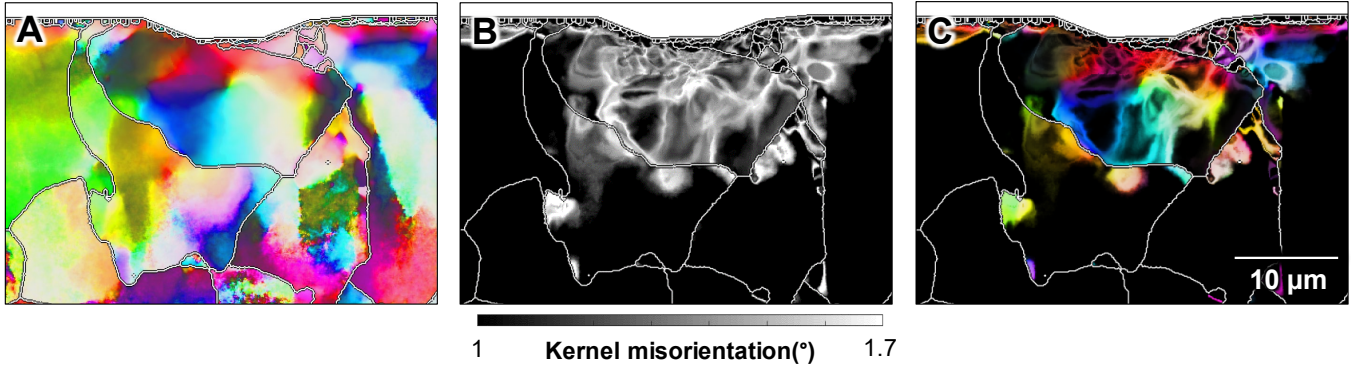
Misorientation analysis

- Misorientation axis in specimen and crystal coordinates

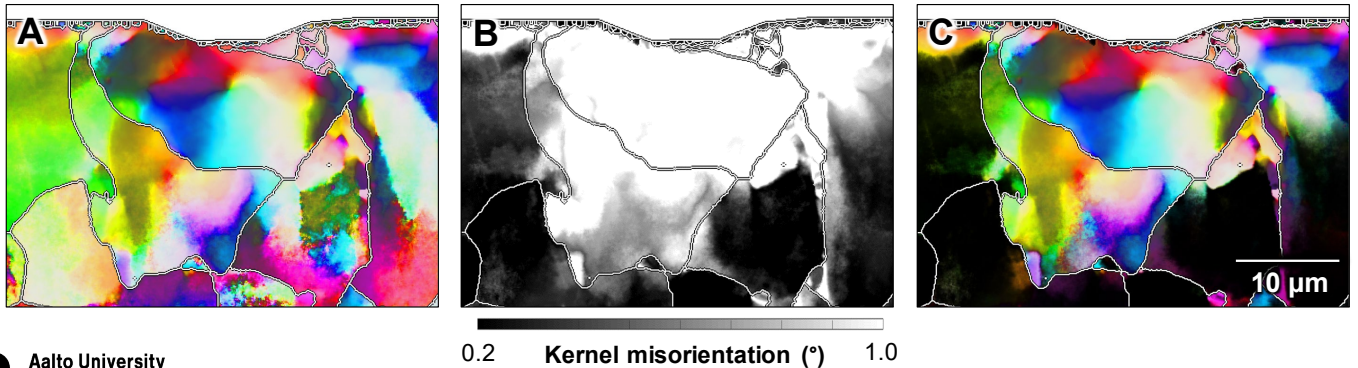


Combination of analysis approaches

- Misorientation axis (SS) + Sub-grain boundaries

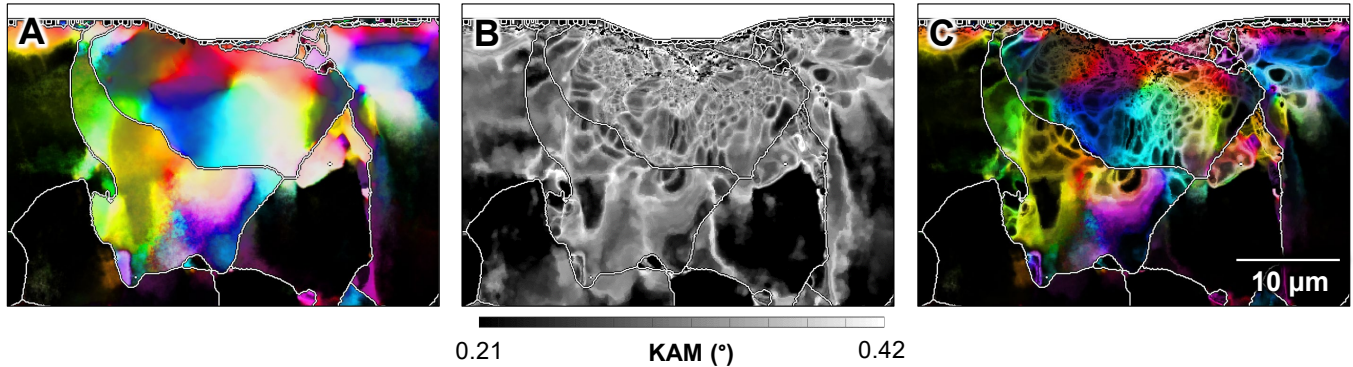


- Misorientation axis (SS) + Extent of plastic deformation

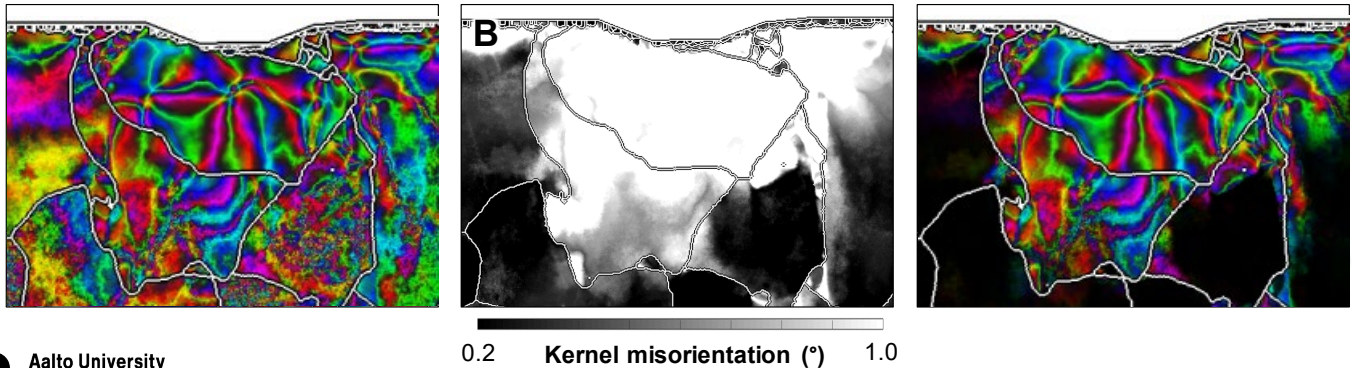


Combination of analysis approaches

- Misorientation axis (SS) including plastic deformation zone + Dense dislocation walls



- Misorientation axis (CS) + Extent of plastic deformation

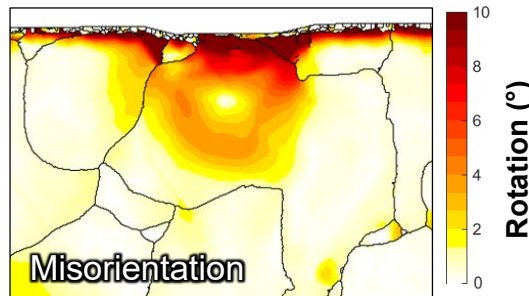
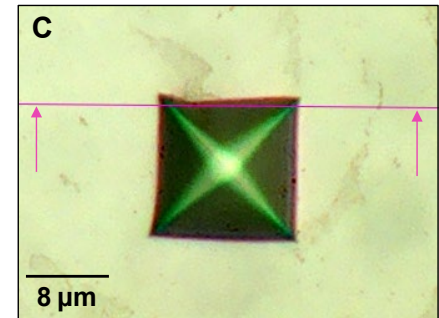
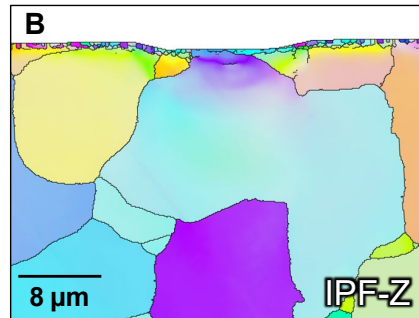


Analysis example #1

Dislocation motion

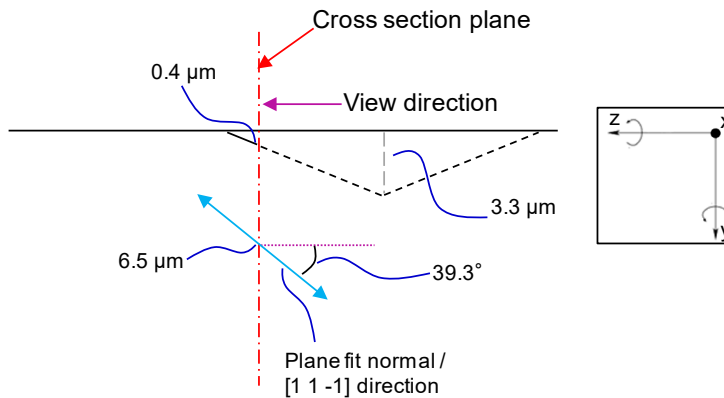
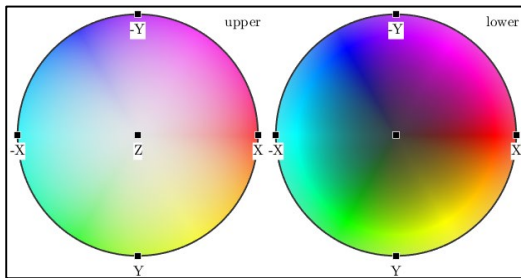
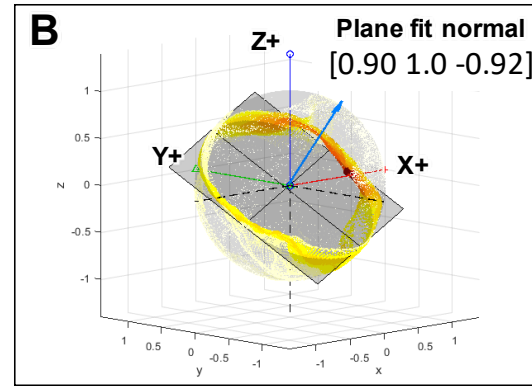
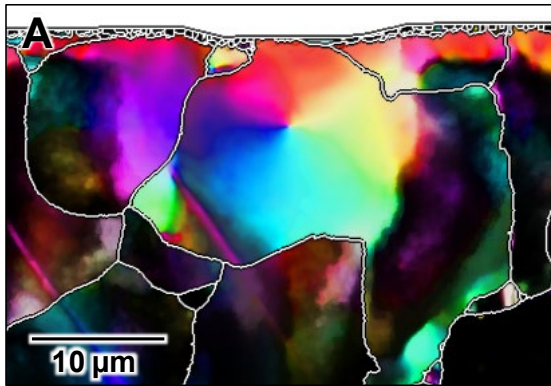
Dislocation motion

- Clustering enables more accurate deformation analysis
- Investigation to resolve what causes local minima in the misorientation field
- Attempt to link dislocation motion with the rotation patterns



Dislocation motion

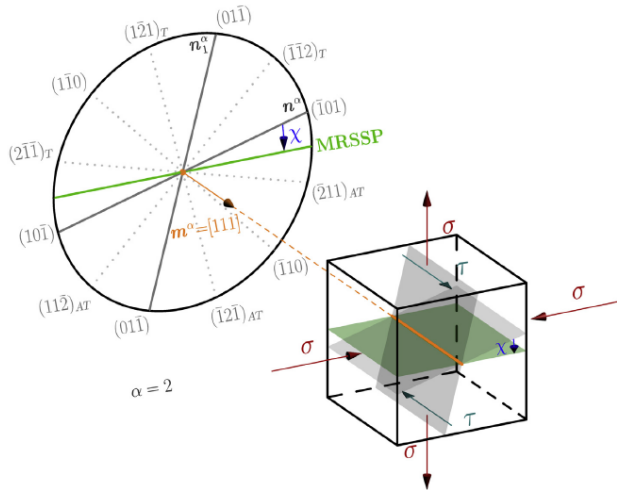
- Misorientation axis distribution (specimen symmetry) shows strong symmetry
- A plane fit to the data reveals a normal vector close to $[1\ 1\ -1]$, indication of dislocation slip direction



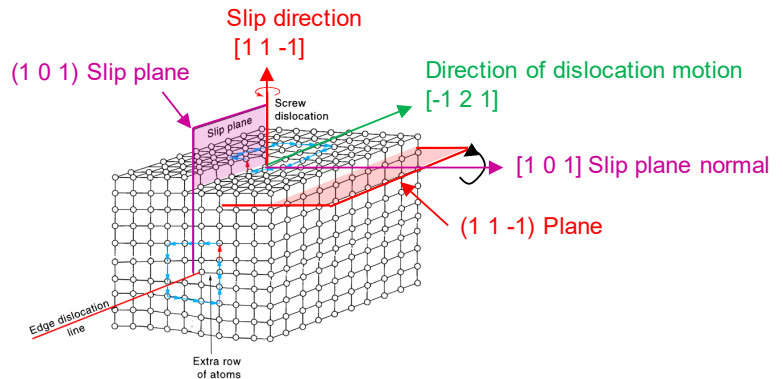
Dislocation motion

- For BCC materials such as the structural steel, the $[11-1]$ direction is a zone axis associated with three $\{110\}\langle 11-1 \rangle$ and three $\{211\}\langle 11-1 \rangle$ slip systems
- Screw dislocations determine the plastic deformation process (below T_c)
- For a screw dislocation with $[11-1]$ slip direction, the dislocations on a $(1\ 0\ 1)$ plane move to the $[-1\ 2\ 1]$ direction

$[111]$ zone axis



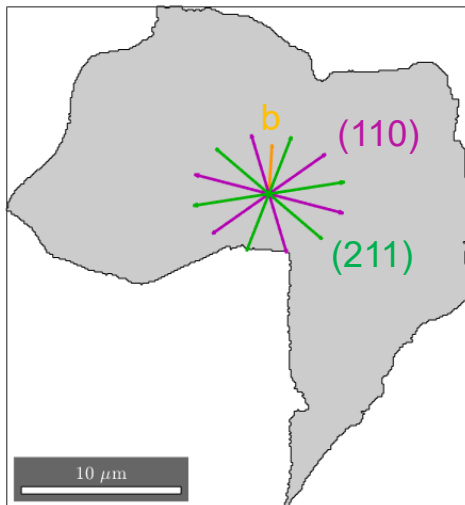
Geometry of dislocation motion for screw dislocation



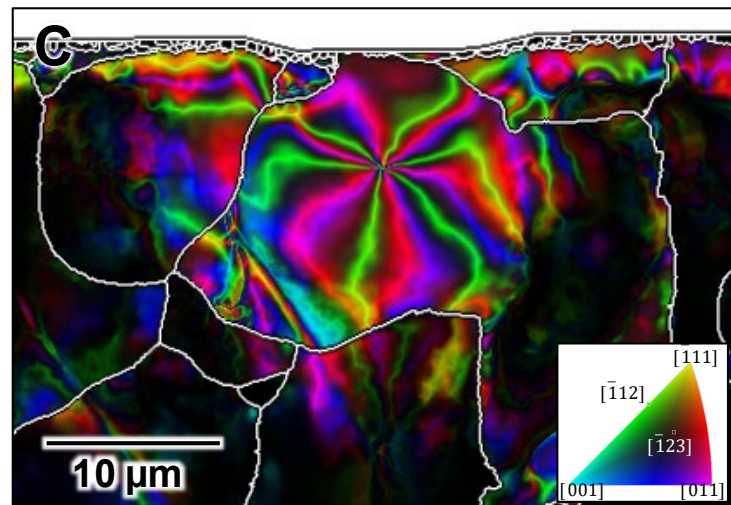
Dislocation motion

- Based on the clustered reference orientation, direction of dislocation motion can be estimated for the $\{110\}$ and $\{211\}$ slip planes
- Experimental result shows traces radiating outward from the misorientation minimum at the centre of the grain

Estimated dislocation motion directions

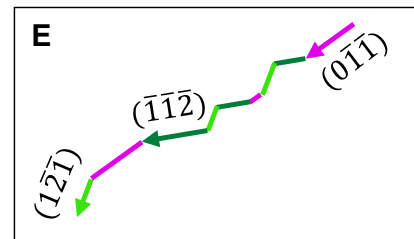
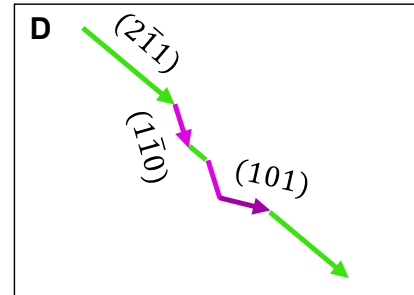
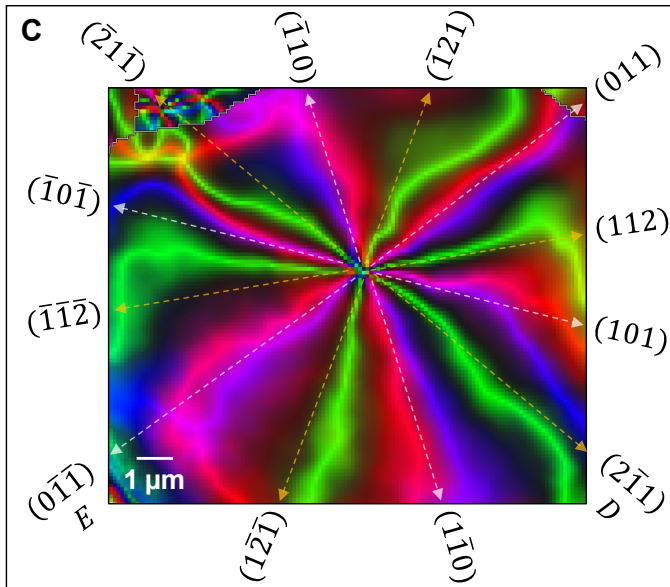


Experimental patterns



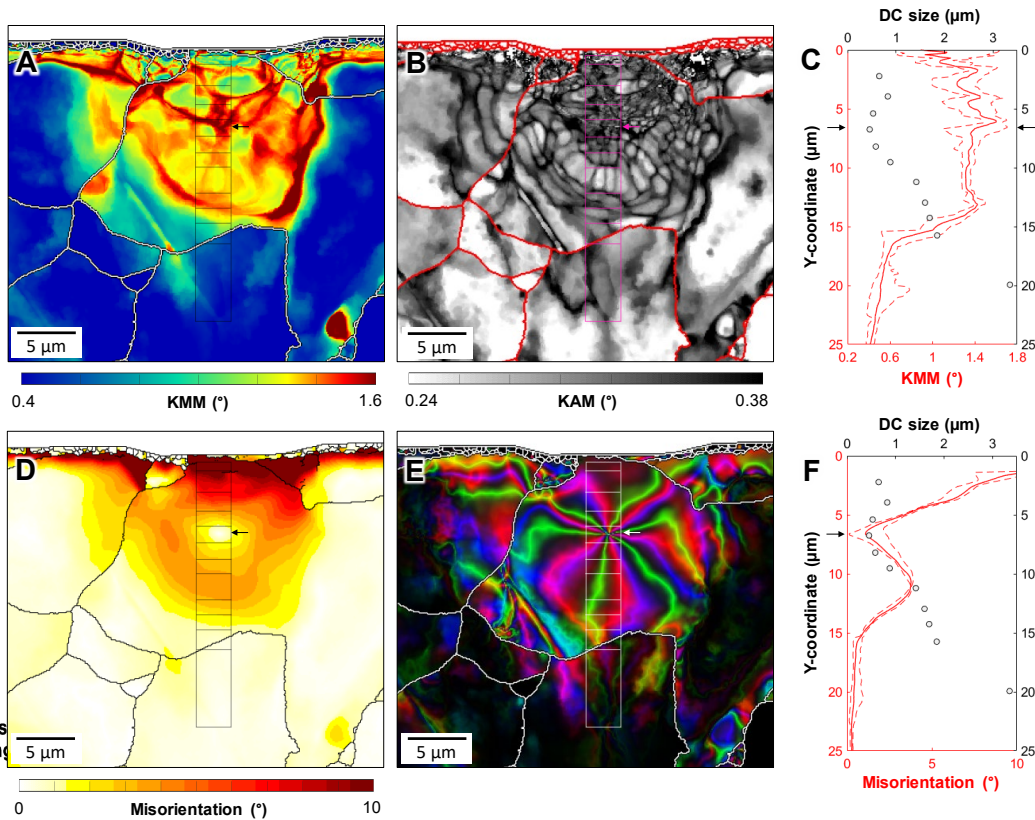
Dislocation motion

- Global direction of the traces is consistent with the estimated directions
- Jagged appearance of the traces indicates cross-slip processes on neighbouring (110) and (211) slip planes, producing macroscopic slip in (211) and (110) slip planes directions



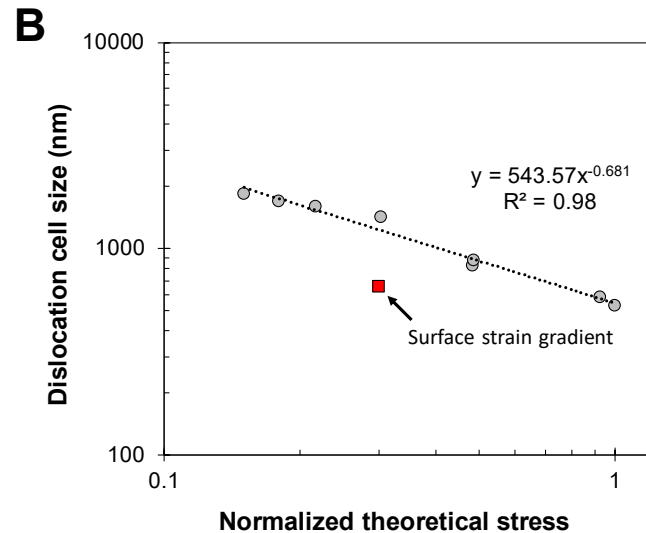
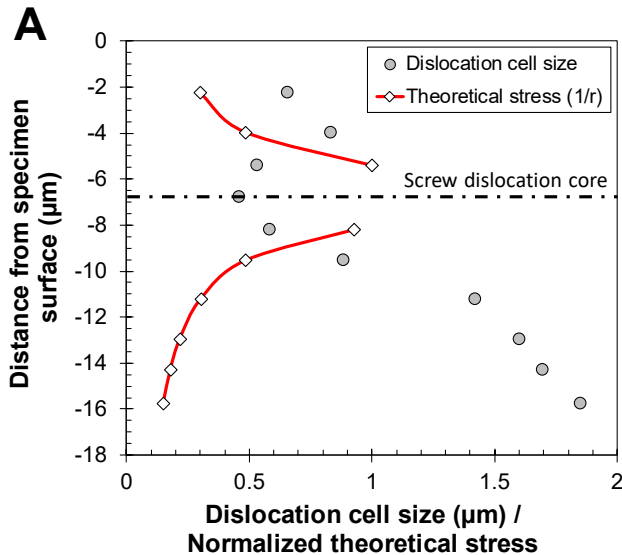
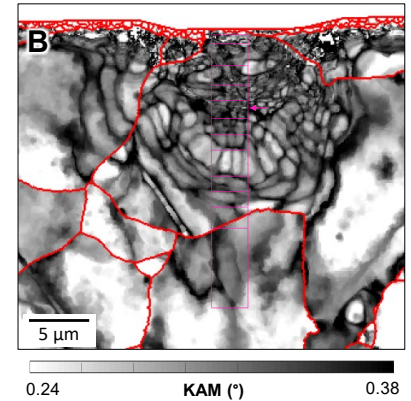
Dislocation motion

- Dislocation cell size is the smallest at the location of the misorientation minimum
- Small dislocation cell size indicates large local stresses and strains



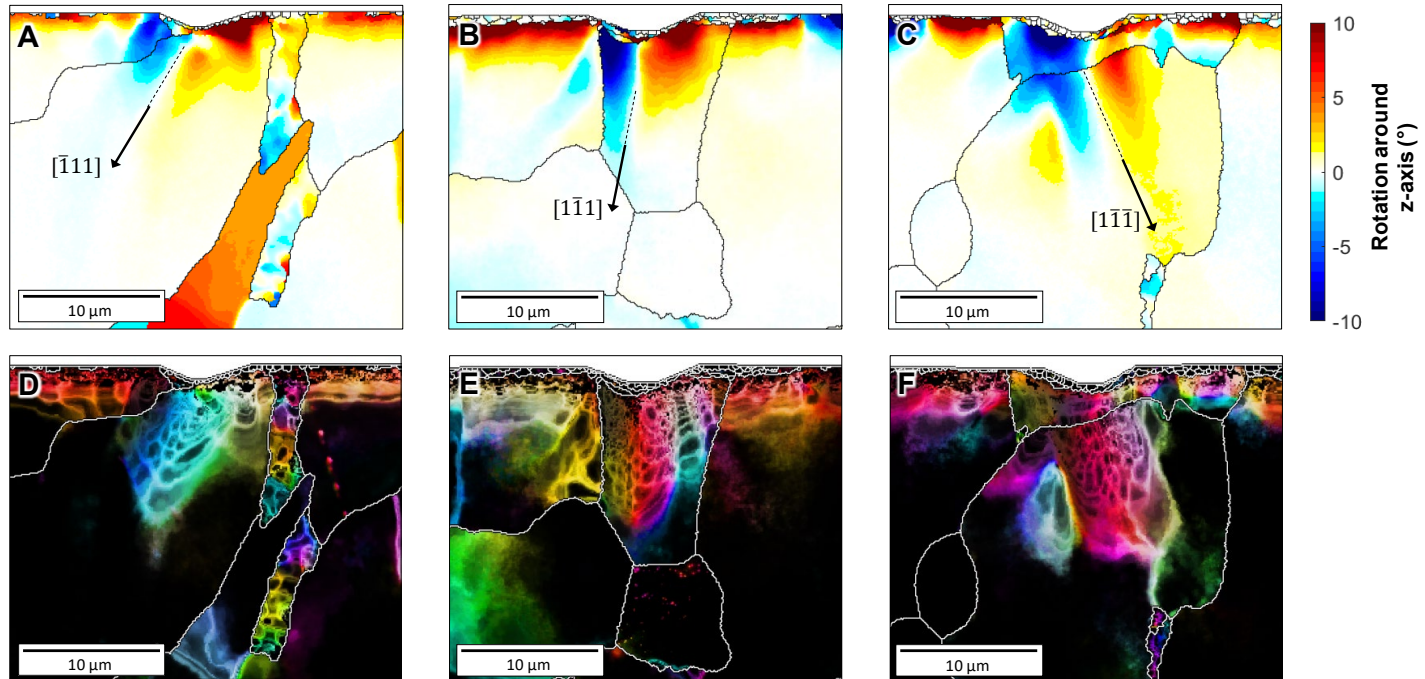
Dislocation motion

- Assuming we are dealing with a screw dislocation, it's stress distribution is inversely proportional to the distance from its core
- With this assumption, the dislocation cell size follows the theoretical stress



Dislocation motion

- Deformation progresses in $\langle 11-1 \rangle$ directions for the studied BCC steels
- Influence of grain boundaries and grain size on slip transmission can be studied

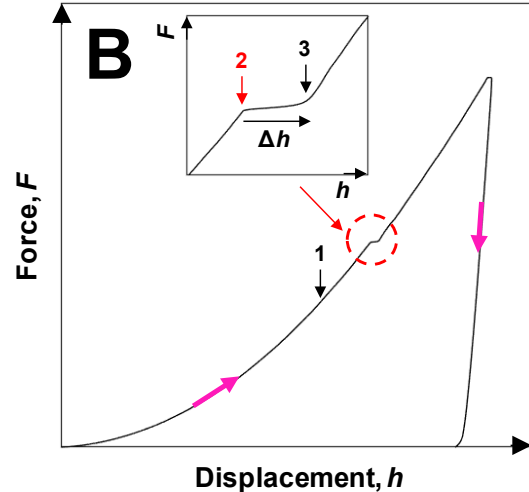
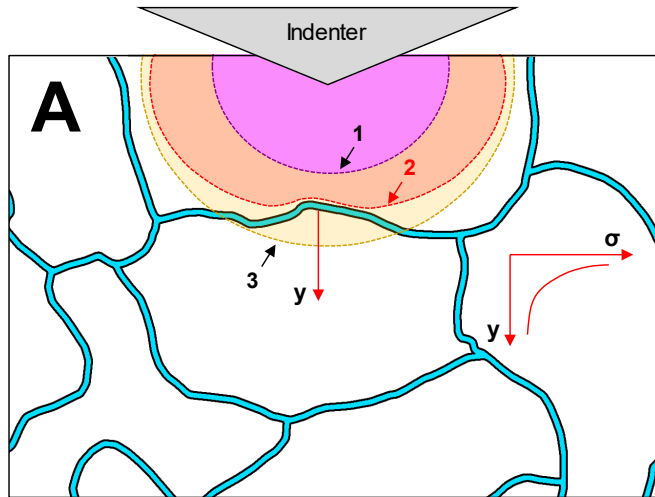


Analysis example #2

Grain interaction

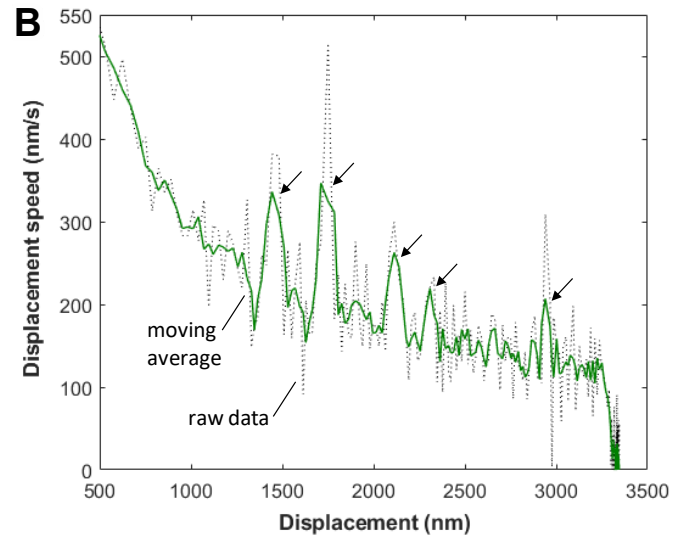
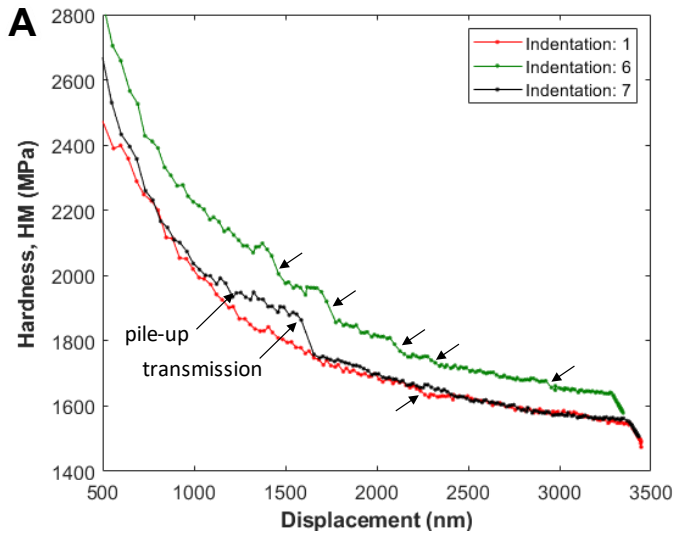
Grain interaction

- As an indenter is pushed deeper into the material, the plastic deformation zone will start to influence multiple grains
- Strain bursts (Δh) during an instrumented indentation test indicate significant dislocation pile-up – slip transmission events at grain boundaries
- As transmission takes place, energy of the pile-up is released, resulting in a temporary increase of indenter's speed of displacement (in a force controlled test)



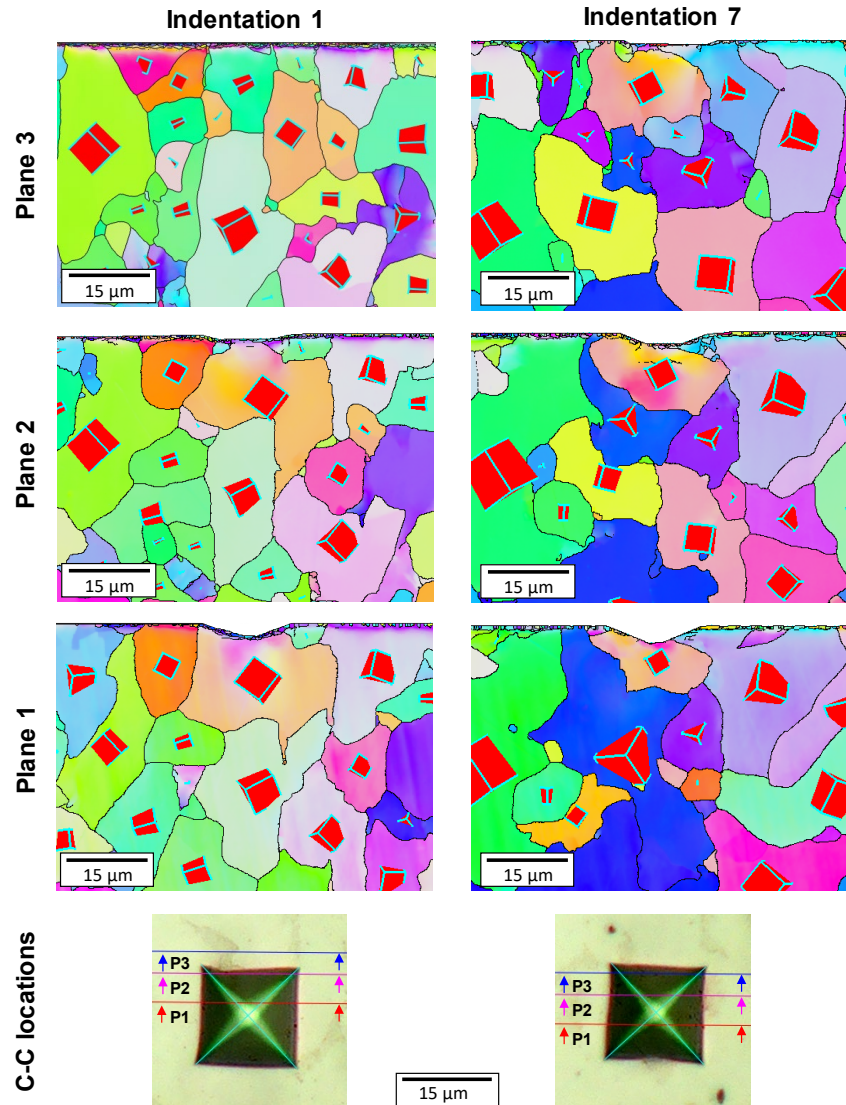
Grain interaction

- When hardness is measured as a function of indentation depth, the changes in displacement speed (B) are visible as drops in hardness (A)
- Three cases:
 - 1) No significant strain bursts (1)
 - 2) One significant strain burst (7)
 - 3) Multiple strain bursts (6)



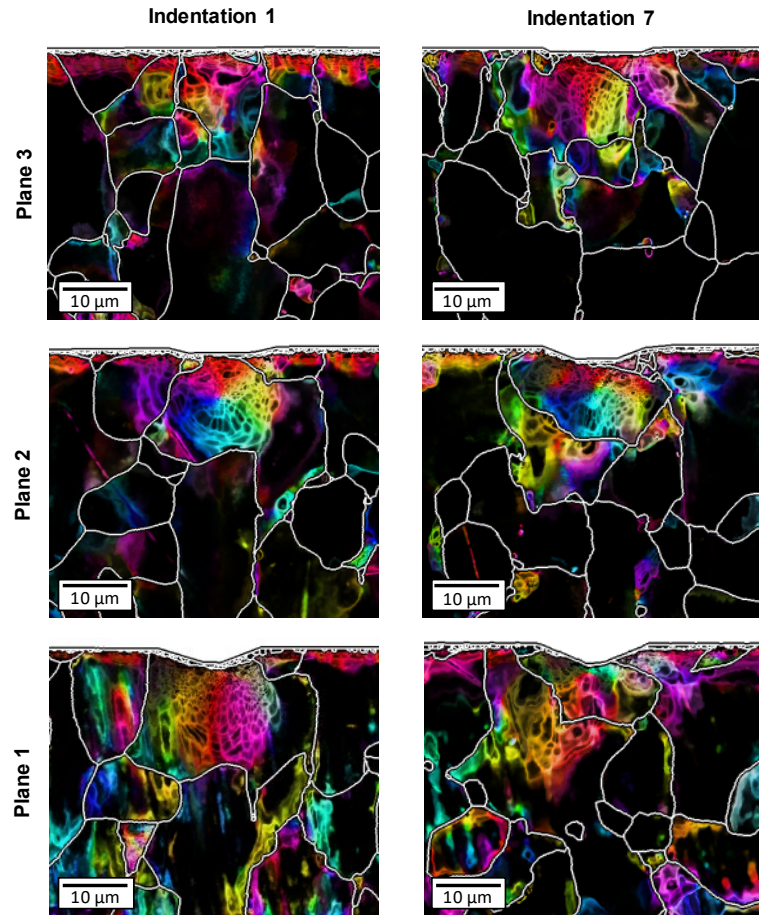
Grain interaction

- Comparison between no bursts (1) and one significant burst (7)
- Similarity of orientation for the large grain under the indenter, with a significantly larger grain size for indentation 1

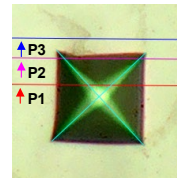


Grain interaction

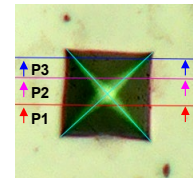
- For indentation 1 the majority of the deformation is contained in the large grain, without transmission taking place from this grain (plane 1 and 2)
- For indentation 7 there is clear transmission from the grain under the indenter visible on planes 1 and 2
 - Most likely slip transmission has taken place near plane 1, as there's continuity of rotation axes (ss) across the GB, and the grain has a sharp corner (stress concentrator)



C-C locations

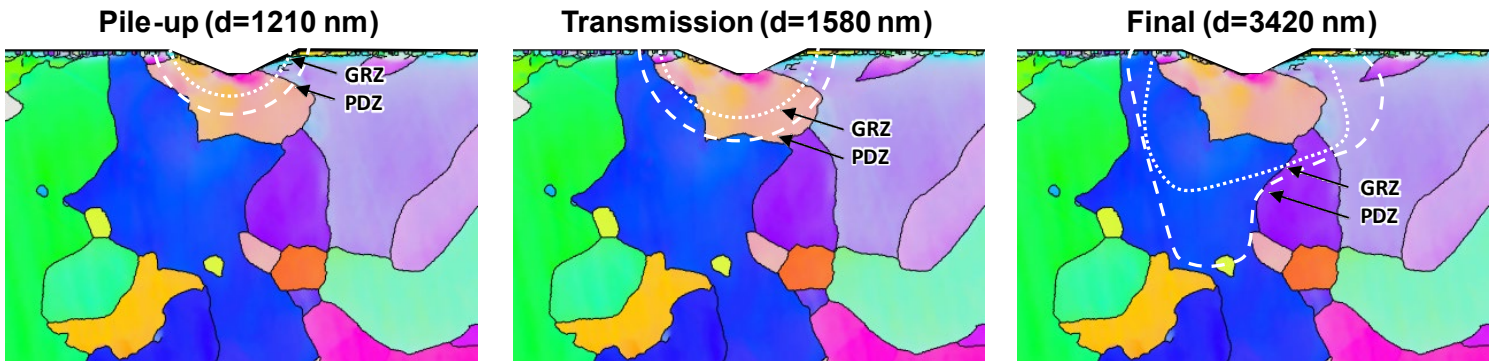


15 μm



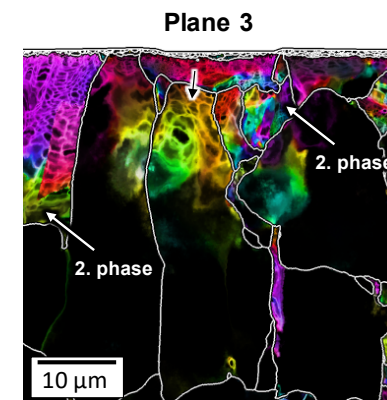
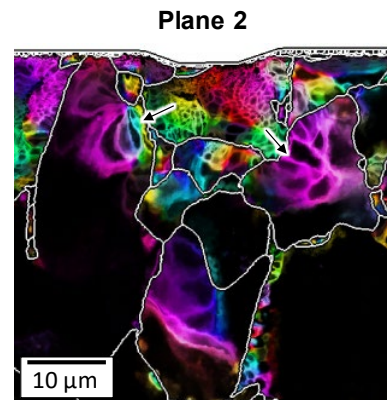
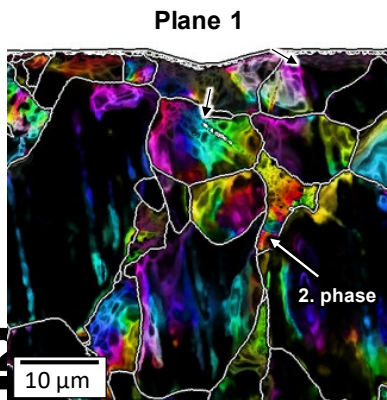
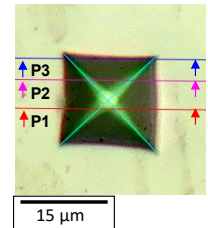
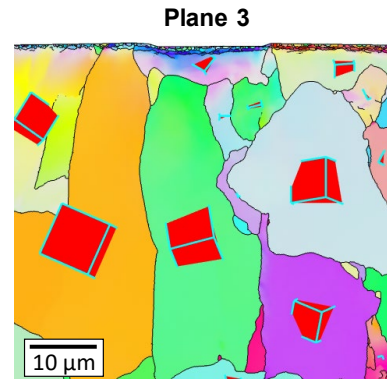
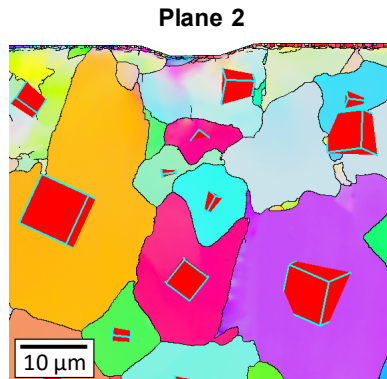
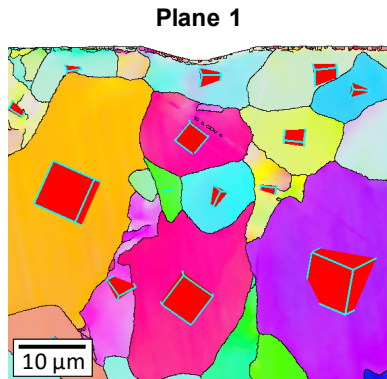
Grain interaction

- The size of the grain refined and plastic deformation zones is estimated for the onset of the pile-up and slip transmission for indentation 7
 - Hemispheric shape assumed for simplicity
- Based on the estimation, pile-up effects are visible when the PDZ reaches the GB.
- Transmission took place approximately when the GRZ reached the GB.



Grain interaction

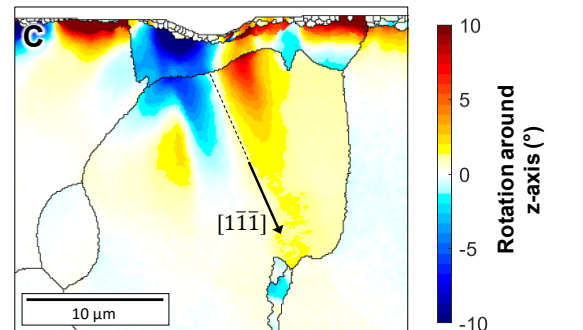
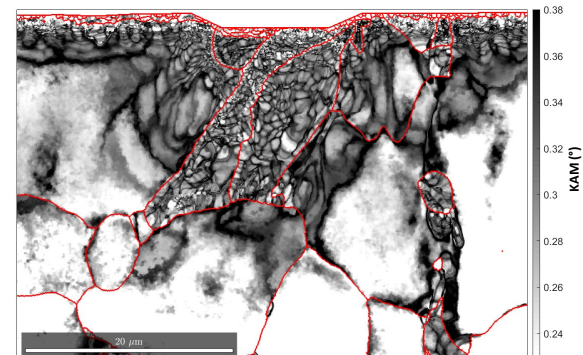
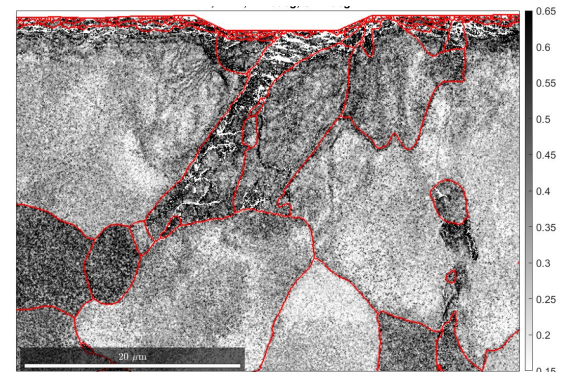
- Indentation 6 has multiple small grains under the indenter
- Misorientation analysis reveals that deformation has been transmitted to multiple grains, consistent with the strain bursts in indentation data



Conclusions

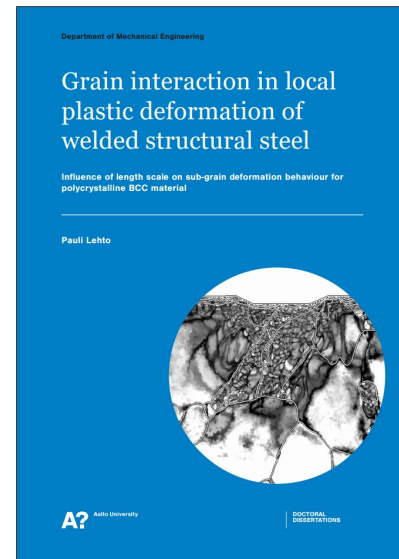
Conclusions

- MTEX is extremely versatile for orientation data post-processing and analysis!
- For plastic deformation analysis even Hough-based EBSD data contains a lot of information when processed and analysed in an efficient manner
- Deformation patterns can be linked with deformation mechanisms



References

- More detailed information on the methods can be found in my doctoral dissertation:
<http://urn.fi/URN:ISBN:978-952-60-8807-5>
- The grain size measurement methods are available at: <http://wiki.aalto.fi/display/GSMUM/>
 - MTEX implementation is future work
- The adaptive kernel misorientation method and clustering based misorientation analysis will be made available as an open source code in due course with example datasets
- **For any questions don't hesitate to contact me at pauli.lehto (at) aalto.fi**



Grain size measurement using Matlab

Created by Pauli Lehto. last modified on Jan 25, 2017

Matlab grain size measurement

This webpage summarizes the work of the author published in Refs. [1] and [2] regarding the characterization of grain size for metallic materials. The methodology for the characterization of grain size and the grain size distribution is explained, and Matlab grain size measurement code is made available for free download. The Matlab code is provided under the GNU General Public License v3 (<http://www.gnu.org/licenses/>). The code is provided as is and can be freely modified. The versions available represent the code used in Ref. [1] for measurement of average grain size and grain size distribution, and Ref. [2] for measurement of local grain size variation. The code requires the Matlab 'Image Processing Toolbox' and 'Statistics Toolbox' to run.

This webpage is divided into two parts. The first summarizes the characterization of average grain size according to Ref. [1], and the second part deals with characterization of local grain size variation [2]. The second part is an extension of the previous work, and thus the same basic principles apply. The updated version of the point-sampled linear intercept length measurement code produces the same result as the previous version, but is significantly faster. In addition, grain size maps with moving averages of grain size can be shown on screen or saved to a file directly.

The Matlab codes are downloadable from here:

- Version 1 of the line and point-sampled intercept length methods
- [1]: [Public_matlab_code_v1.zip](#)
- Version 2 of the point-sampled intercept length method [2]: [Public_matlab_code_v2h.zip](#)

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- Lehto, P.; Remes, H.; Saukkonen, T.; Hänninen, H.; Romanoff, J. Influence of grain size distribution on the Hall-Petch relationship of welded structural steel, *Materials Science and Engineering: A*, 2014; 592: 28-39, <http://dx.doi.org/10.1016/j.msea.2013.10.094>
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